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**CONCEPTUAL DESIGN
FOR THE FINAL FOCUS QUADRUPOLE MAGNETS
FOR TESLA**

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ABSTRACT

We present a preliminary design of the superconducting final focusing quadrupole magnets for TESLA and all their associated cryogenics.

1	INTRODUCTION	1
2	ELECTROMAGNETIC DESIGN	2
3	MECHANICAL DESIGN	5
3.1	Overview	5
3.2	Numerical Model	6
3.3	Results	10
3.4	Conclusions	13
4	CABLE SPECIFICATION	13
5	CRYOGENICS	15
5.1	Overview	15
5.2	Cryostat	15
5.3	Refrigeration	16
5.4	Heat loads	17
	REFERENCES	19

1.....INTRODUCTION

The Tera Electron volts Superconducting Linear Accelerator (TESLA) is an electron/positron linear collider, with an energy of 250 GeV per beam, under consideration at the Deutsches Elektronen Synchrotron (DESY) [1]. Two superconducting magnet systems are required in the TESLA interaction region where the beams cross with a zero angle: (1) a set of four final focusing quadrupole magnets (two on each side of the collision point) and (2) a large solenoid embedded in the detector array (surrounding the collision point). To benefit from the experience and the development work carried out for the Large Hadron Collider (LHC), presently under construction at the European Laboratory for Particle Physics (commonly referred to as CERN) [2], the design of the two magnet systems is based on existing LHC designs: the final focusing quadrupole magnets are modeled after the LHC arc quadrupole magnets [3], and the solenoid is modeled after the Compact Muon enoid (CMS) that will be implement in one of LHC experiments [4].

There is at least one major difference between TESLA and LHC: for beam optics reasons, the TESLA final focusing quadrupole magnets must be localized very close to the interaction point. As illustrated in Figure 1, they end up inside the solenoid and must operate in its background field. Given the field requirements (4 T for the solenoid and 250 T/m within an aperture of 56 mm for the quadrupole magnets), we are at the limit of NbTi cable performances and it is more appropriate to consider Nb₃Sn cables.

The present note describes a preliminary conceptual design of the final focusing quadrupole magnets for TESLA, which is based on the LHC arc quadrupole magnet design, but relies on Nb₃Sn cables. The main goals are: to set a cable critical current specification, and to dimension the coil support structure and cryostat.

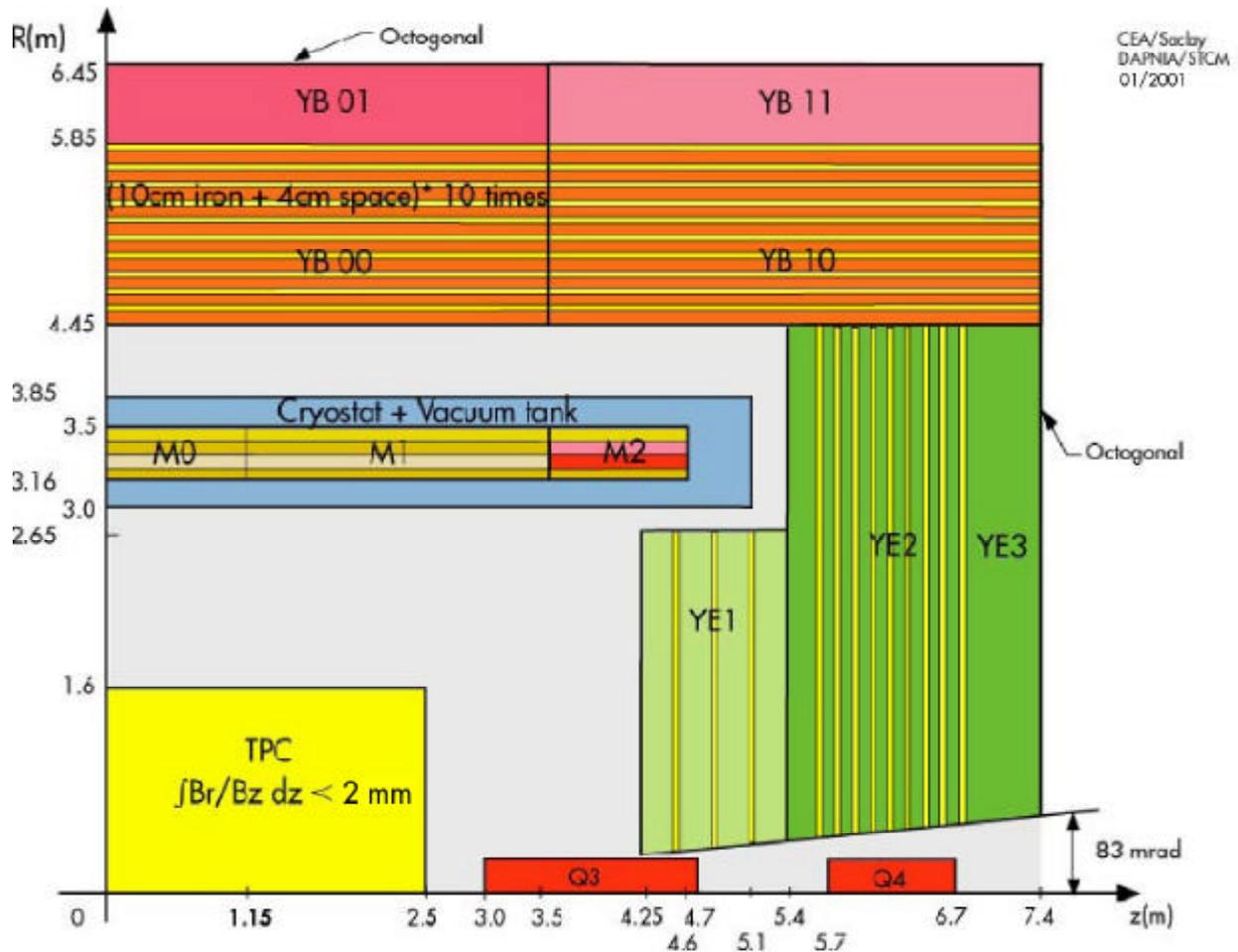


Figure 1 Layout of TESLA interaction region showing the final focusing quadrupole magnets (Q3 and Q4) inside the detector solenoid (M0, M1 and M2).

2..... ELECTROMAGNETIC DESIGN

As mentioned above , the electromagnetic design of the TESLA final focusing quadrupole magnets rely on the same four coils and the same conductor geometries as for the LHC arc quadrupole magnets, but it has no iron yoke (for it would be of no use in the solenoidal field). The conductor layout is presented in Figure 2. The two layers are wound from the same cable, which is based on LHC quadrupole magnet cable specifications [5]. The inner layer counts 10 turns divided in two blocks by an angular wedge, and the outer layer counts 14 turns, also divided in two blocks by an angular wedge.

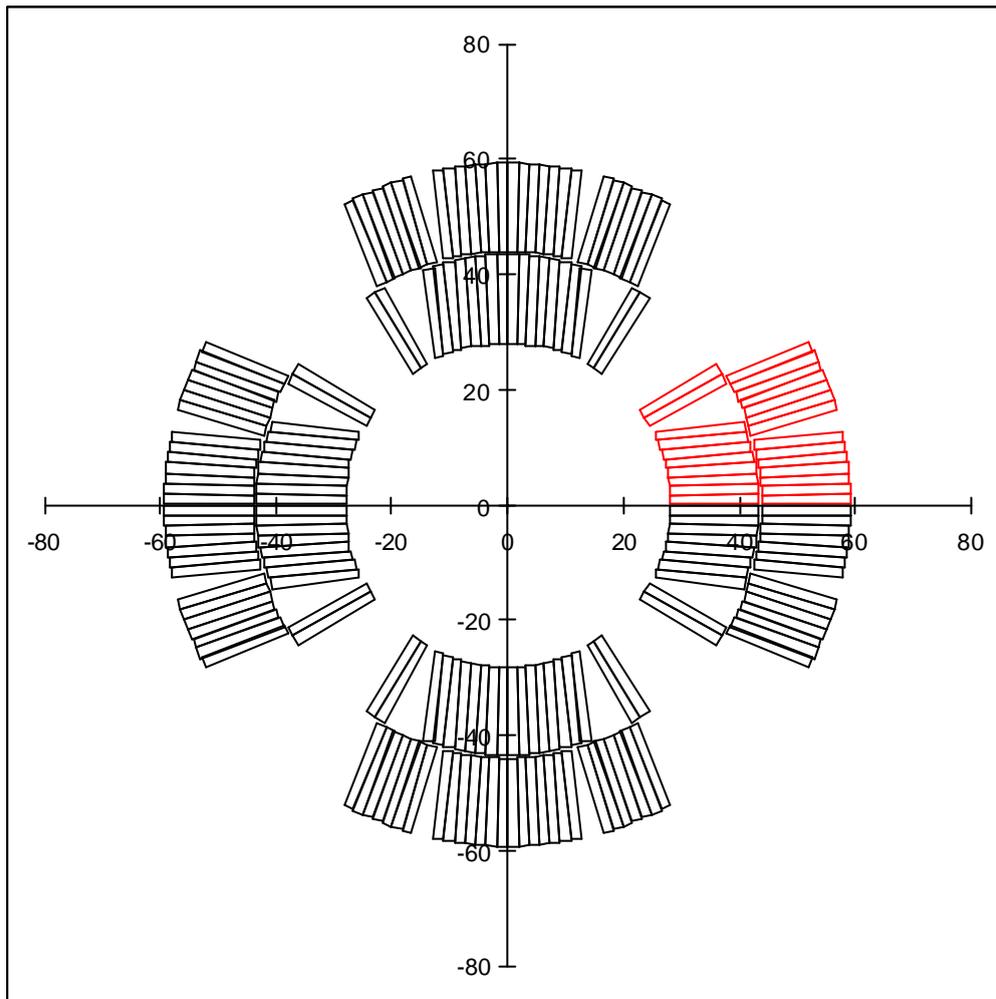


Figure 2 Conductor layout of LHC arc quadrupole magnets.

One possible difference between the TESLA and LHC quadrupole magnet designs could be the conductor insulation thickness. In the case of LHC NbTi cables, the insulation is made up of polyimide tapes and is estimated to be 110 μm per conductor face under 70 MPa. In the case of TESLA Nb₃Sn cables, the insulation will rely on more fragile mineral fiber tapes and may have to be thicker (DAPNIA/STCM is currently developing a quartz fiber tape that could yield a minimum of 120 μm per conductor face [6]). This over-thickness can be compensated by removing the wedge insulation and/or by reducing the conductor mid-thickness. For the present, preliminary computations, we consider the conductor layout of the LHC arc quadrupole magnets as it is now.

In this design, the quadrupole field gradient, g , can be estimated as a function of supplied current, I , using

$$g = 17.7747 \cdot 10^{-3} I \quad (1)$$

From Eq. (1), it follows that the current, I_{op} , corresponding to an operating field gradient of 250 T/m is

$$I_{op} \approx 14,065 \text{ A} \quad (2)$$

In order to operate the quadrupole magnets with a margin of 20% along the load line, the cable critical current, I_C^{cable} , must satisfy

$$I_C^{cable} \geq \frac{I_{op}}{0.8} \approx 17,581 \text{ A} \quad (3)$$

Furthermore, the peak magnetic flux density on the magnet coil when the quadrupole magnet stands alone, B_p , can be estimated from

$$B_p \approx 0.5436 \cdot 10^{-3} I \quad (4)$$

and it follows that the peak magnetic flux density, $B_{p,C}$, corresponding to the lower limit of I_C^{cable} is simply

$$B_{p,C} \approx 9.56 \text{ T} \quad (5)$$

When the quadrupole magnet is positioned inside the detector magnet, it seems reasonable to assume that (at least in the quadrupole magnet straight section) the two magnetic flux densities add up quadratically, as the two fields are roughly orthogonal.

Hence, the superconducting cable must be specified to carry the current I_C^{cable} under a magnetic flux density, B_{spec} , derived from

$$B_{\text{spec}} \approx \sqrt{9.56^2 + 4^2} \approx 10,36 \text{ T} \quad (6)$$

3..... MECHANICAL DESIGN

3.1 OVERVIEW

The magnet coils will be produced according to the “wind, react & impregnate” technique. Prior to winding, the un-reacted Nb₃Sn cable will be wrapped with a mineral fiber tape. Upon winding completion, the whole coil will be subjected to the heat treatment required for Nb₃Sn compound formation (typically: 660 °C for 240 hours). After heat treatment, the coil will be vacuum-impregnated with epoxy resin. It is worth mentioning that an alternative insulation scheme is being investigated by DAPNIA/STCM, that may eliminate the need for a vacuum-impregnation, but the design and the computations reported here correspond to the standard (mineral fiber tape + epoxy resin) scheme.

As in LHC arc quadrupole magnets, the coils will be restrained by laminated, 2-mm-thick, austenitic steel collars locked around them by tapered keys. However, unlike in LHC arc quadrupole magnets, there will be no iron yoke and the collared-coil assembly will be centered directly within a precisely-machined, steel inertia tube delimiting the region of liquid helium circulation. A sketch of the quadrupole magnet cold mass is shown in Figure 3 (note that the radial dimensions are not final).

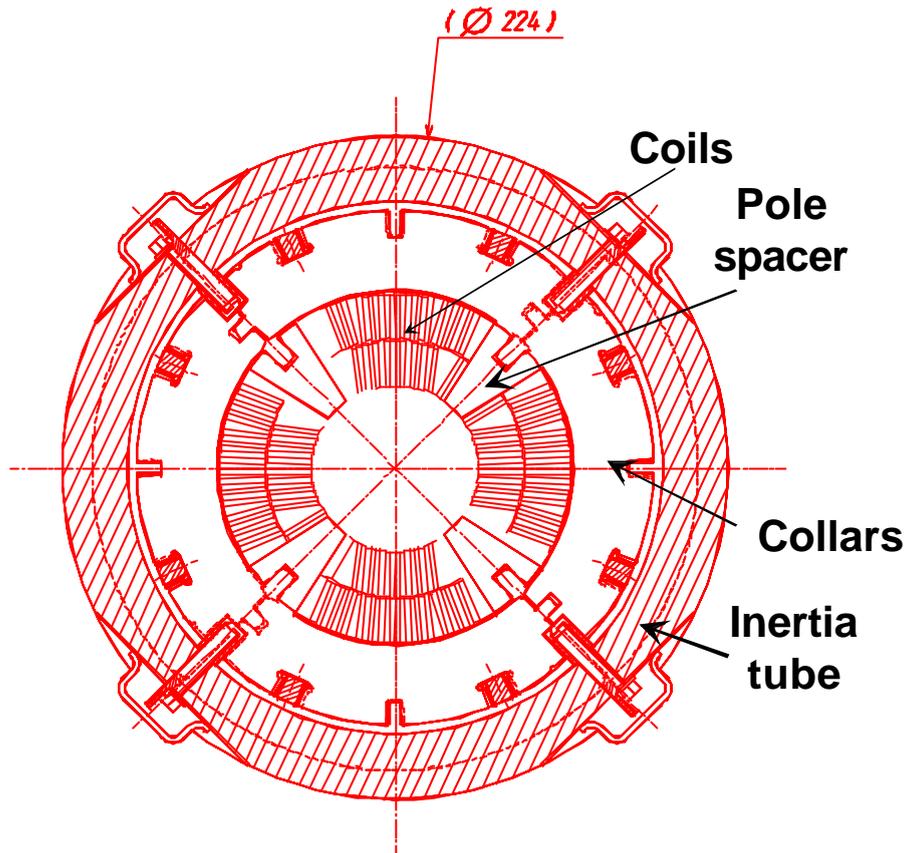


Figure 3 Sketch of quadrupole magnet cold mass (note that the radial dimensions are not final).

We shall now report on a number of mechanical computations, which have been carried out to dimension the coil support structure. The objectives of the mechanical design are [8]: (1) all parts of coils should remain in compression at nominal current, (2) peak stress in coils should be less than 150 MPa at all time, and (3) collar deflections and stress under various loading conditions should not exceed those of the LHC arc quadrupole magnets.

3.2 NUMERICAL MODEL

For this study, we have used a modular approach which is dedicated to the analysis of such complex situations involving 3D assemblies. It is referred to as "COFAST3D" (Contact and Friction in Assemblies of 3D Structures) approach. The COFAST3D approach is based on both a formulation and a strategy which have been developed by Laboratoire de Mécanique et Technologie (LMT) de l'Ecole Normale Supérieure (ENS) de Cachan [7].

The model under study is restricted to 1/4th of the quadrupole magnet cross section. It includes two levels of collars, two keys, four stripping keys, the insulation, the angular and polar wedges and the Nb₃Sn conductor blocks (see Figure 4). Friction is considered on all contact zones (see Figure 5). A 3D mesh of the structure has been developed (see Figure 6).

The mechanical loading can be divided into three different parts corresponding to the history of the superconducting magnet assembly and operation: (1) pre-loading applied during assembly process, (2) cool down from 293 K to 4.2 K, and (3) Lorentz force application during energization.

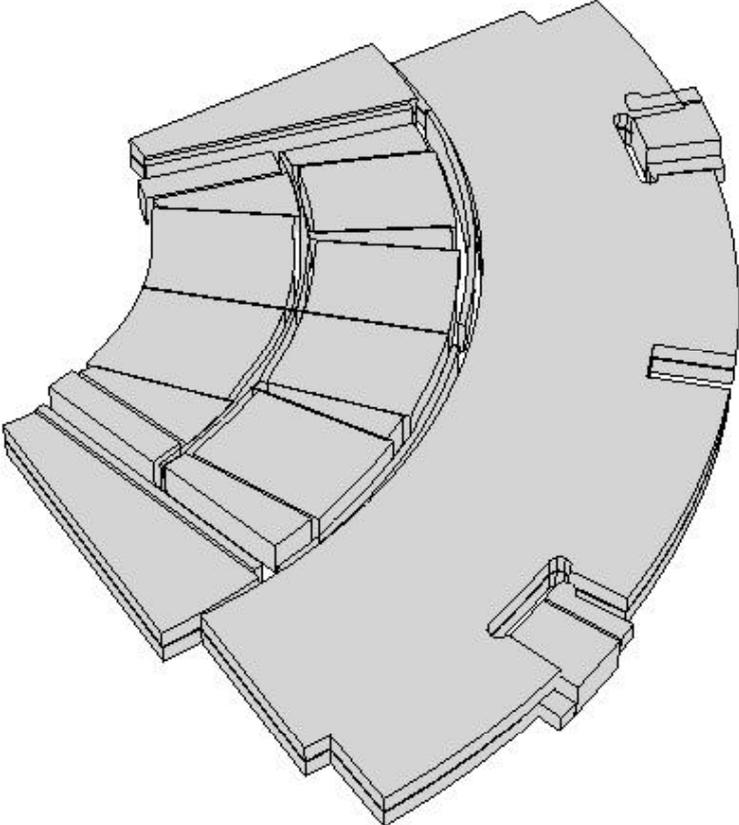


Figure 4 Sub-structure of quadrupole magnet model.

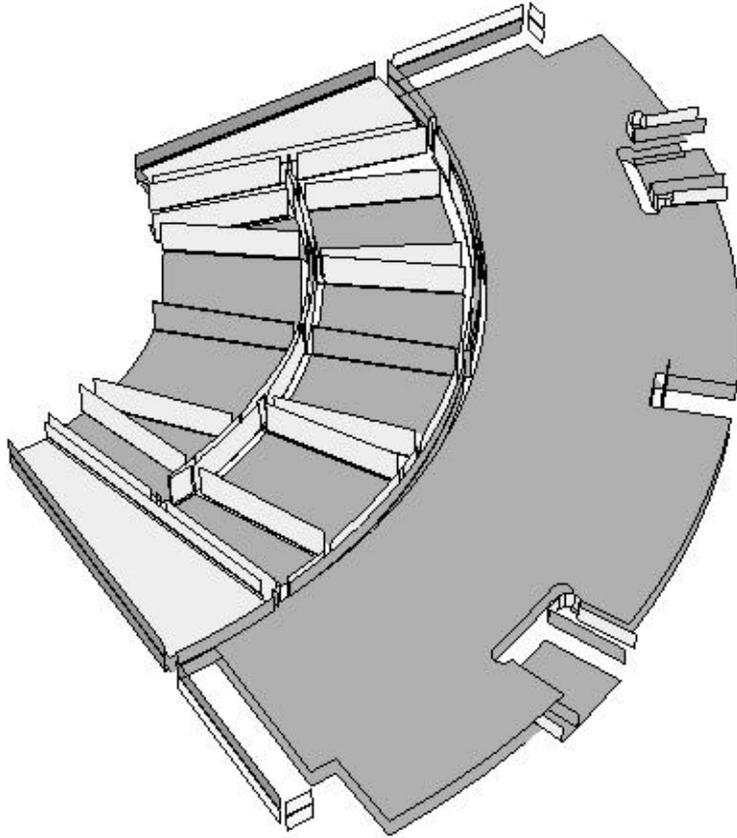


Figure 5
Interfaces of quadrupole magnet model.

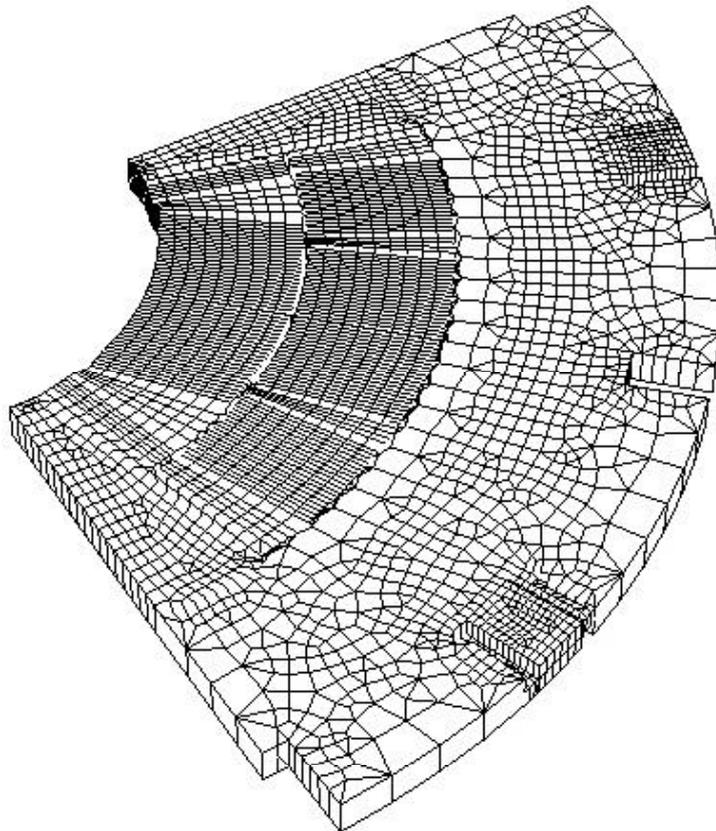


Figure 6
Mesh of quadrupole magnet model.

The magnet assembly corresponds to a two-step collaring process. The first step is modeled by applying surface forces onto the bottom of the collar keyways along the pole axes, while the second step is modeled by imposing a gap between the sides of the keys and the stripping keys. Its correspond to the insertion of the keys into collar keyways.

Cooling is modeled by applying a thermal body force over the entire structure. Note that the temperature distribution is assumed to be uniform throughout cool-down.

Afterwards, the Lorentz forces are modeled by a pre-computed body force field on the coil. Two types of Lorentz forces are induced in the TESLA final focusing quadrupole magnets. The first type is due to the combination of the quadrupole magnetic field and the supplied current, while the second type is due to the combination of the solenoid magnetic field and the supplied current in the end parts of the quadrupole magnet coils.

The Lorentz forces induced during energization when the quadrupole magnet stands alone (without solenoidal background field) can be derived in the usual manner. The components of theses Lorentz forces integrated over a coil octant are: $F_x = 556 \text{ kN/m}$ and $F_y = -989 \text{ kN/m}$ at 14000 A (see Figure 7).

The additional Lorentz forces induced by the solenoidal field are localized in the end parts of the coils. They can be estimated using some assumptions. Integrated over a coil octant, we get: $F_r = \pm 1192 \text{ kN/m}$ at 14 000 A and 4 T (see Figure 7).

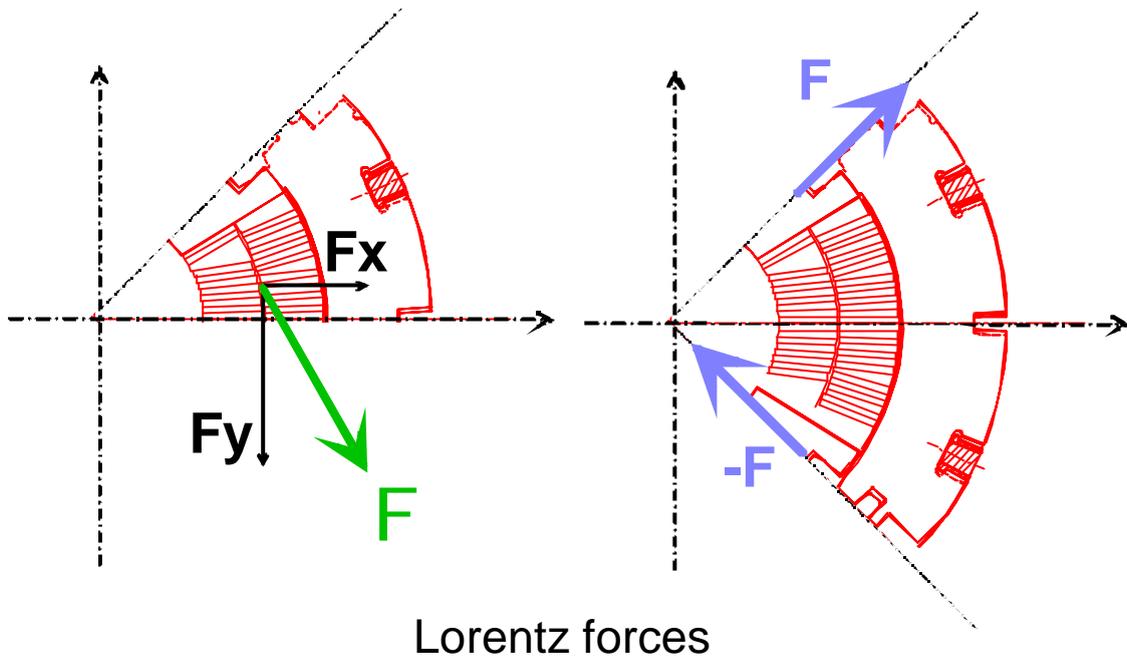


Figure 7
Components of the Lorentz forces on quadrupole magnet coils.

3.3 RESULTS

In this discussion, we only present the final results of the computation, when the magnet is fully energized.

At 14000 A and without solenoidal magnetic field, all parts of coils remain under compression. The external collar radius must be increased to 93.5 mm to minimize collar deflections. With this radius value, the deflections are similar to those obtained on LHC arc quadrupole magnets ($d_{\text{radial}} = -0.013$ mm, compared to $d_{\text{réf}} = -0.010$ mm). In addition, the peak stress in the collars remain under the ultimate stress of austenitic steel ($s_{\text{VM}} = 1000$ MPa for $s_{\text{ult}} = 1600$ MPa). Figure 8 and Figure 9 show plots of the azimuthal stress distribution in the magnet coils and of the Von Mises stresses in the collars at 14000 A, while Figure 10 and Figure 11 present plots of the radial deflections.

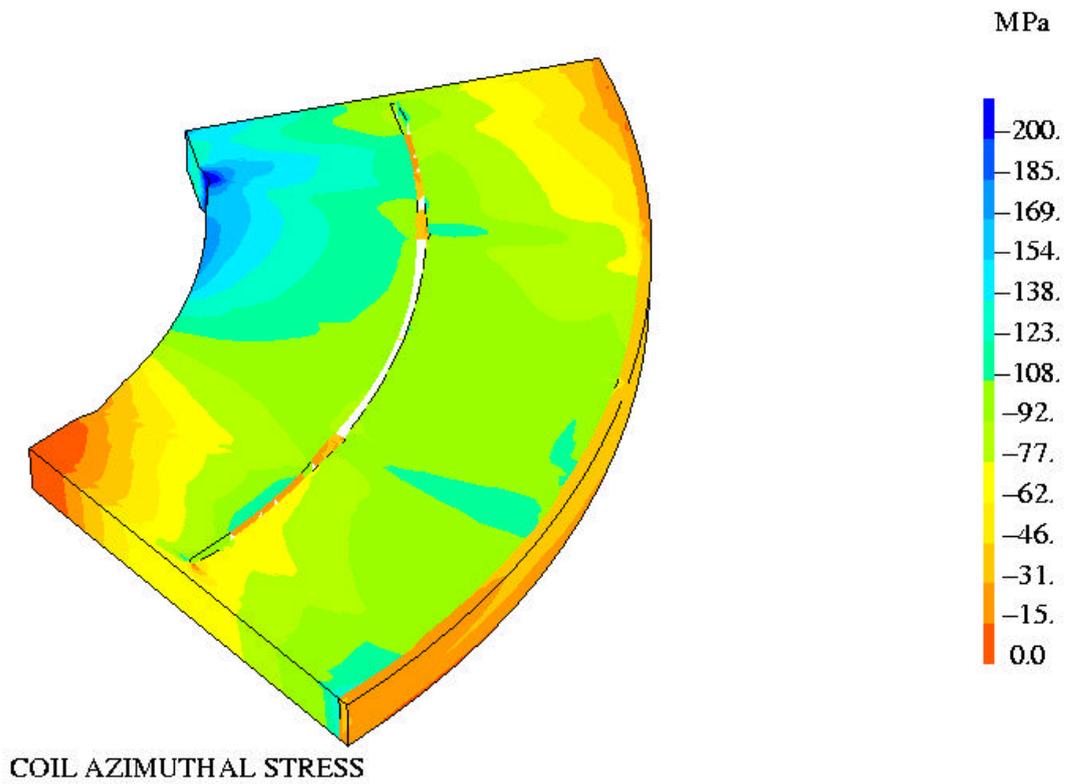


Figure 8
Azimuthal stress distribution in quadrupole magnet coils at 14000 A (without solenoidal field).

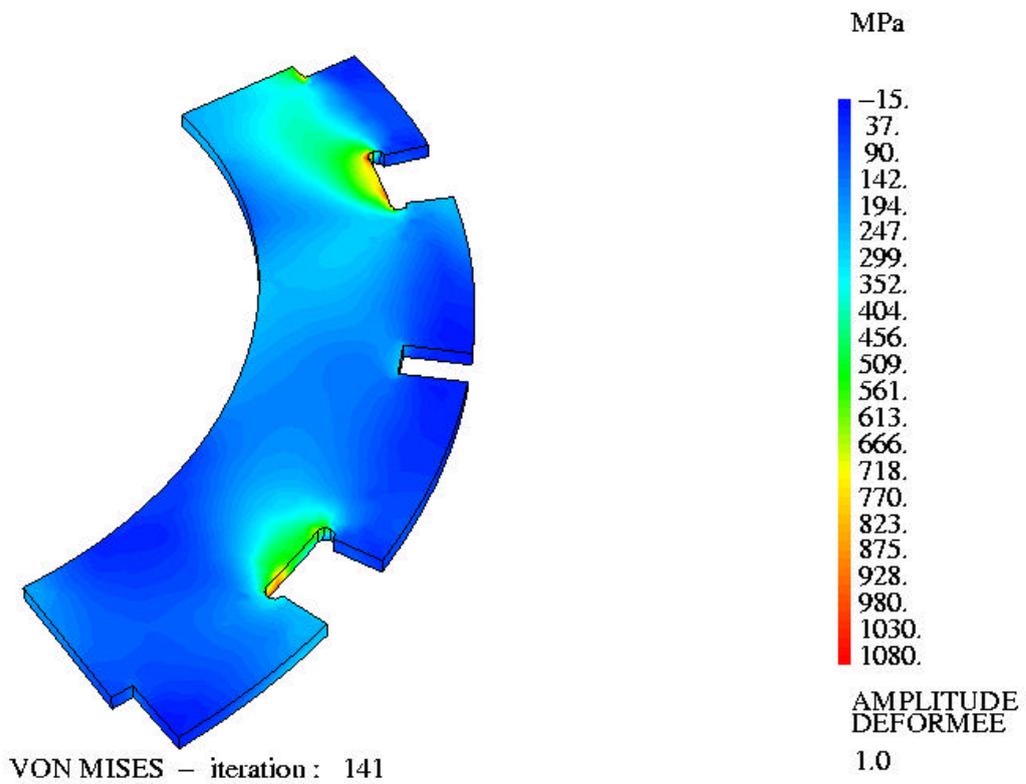


Figure 9
Azimuthal stress distribution in quadrupole magnet collars at 14000 A (without solenoidal field).

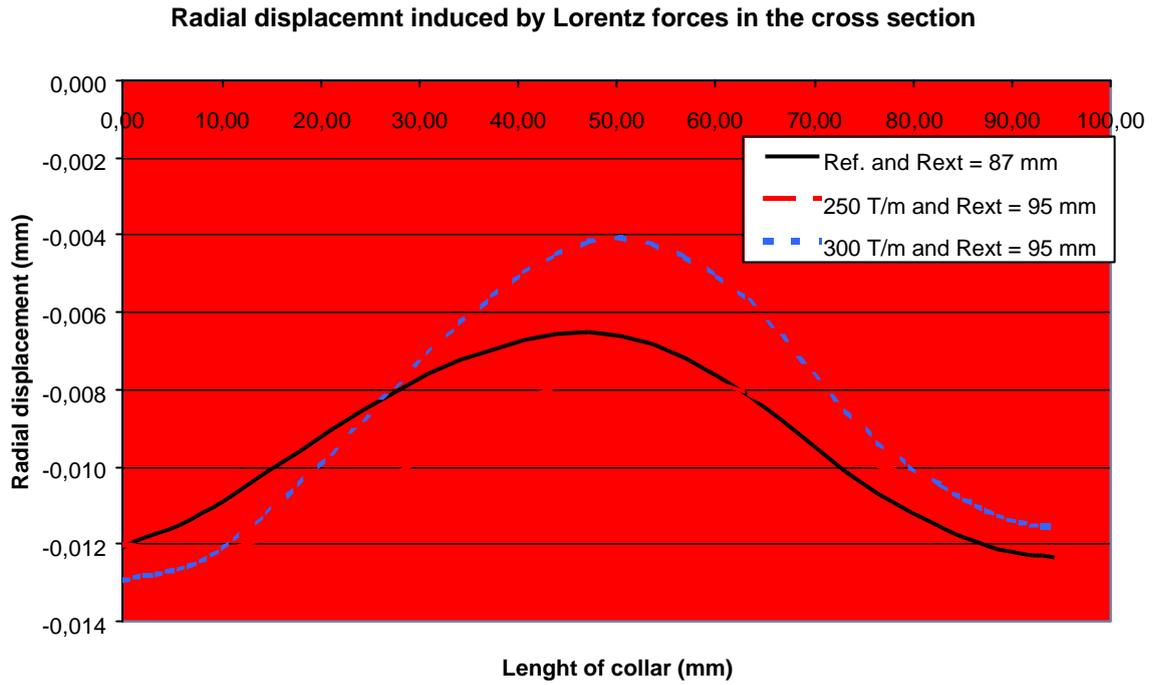


Figure 10
Radial displacements induced by Lorentz forces in 2D cross section at 14000 A and without solenoidal field.

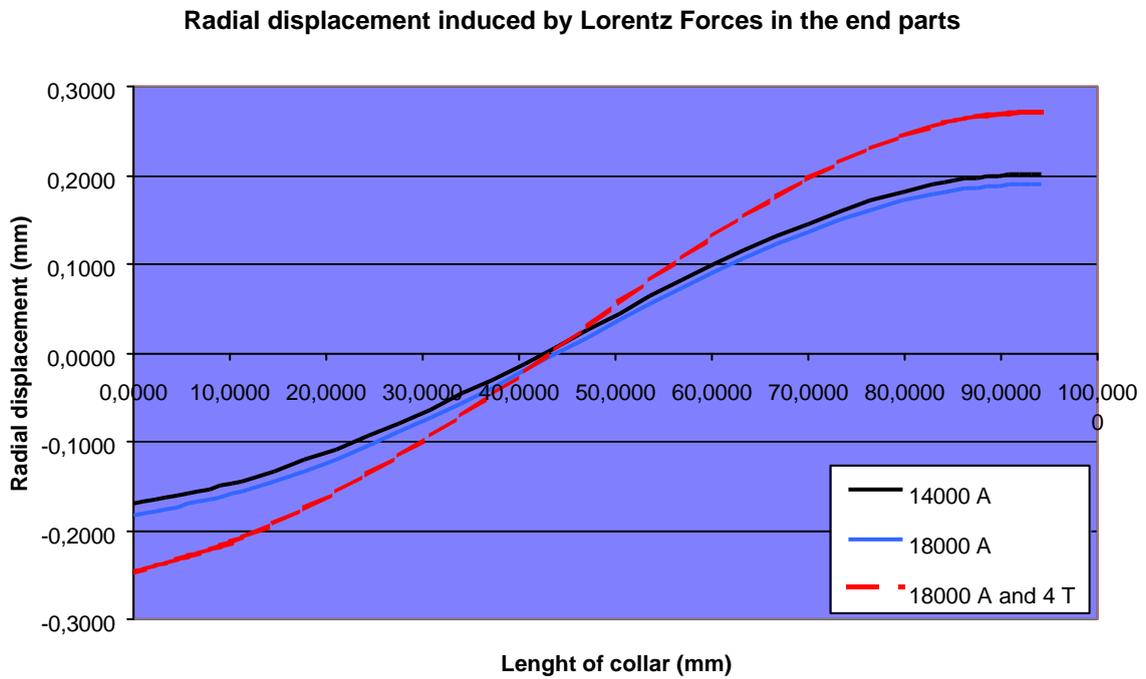


Figure 11
Radial displacements induced by Lorentz forces in coil end parts with and without a 4 T solenoidal field.

At 14000 A and with a 4 T solenoidal magnetic field, all parts of coils still remain under compression, but the radial deflections become very large ($d_{\text{radial}} = \pm 0.2$ mm). Hence, an additional mechanical support will be needed to prevent any damage or to restrain coil end deflections. The peak stress in the collars remain under the ultimate stress ($\sigma_{\text{VM}} = 1250$ MPa for $\sigma_{\text{ult}} = 1600$ MPa).

3.4 CONCLUSIONS

All parts of coils remain in compression at nominal current and with background magnetic field.

The finite element computations validate the main features of the mechanical design, providing that the collar radius is greater than 95 mm and that reinforcements are implemented on the inner and outer radius of the coil ends. With this new value of collar outer radius, it follows that the external radius of the inertia tube must be greater than 110 mm (use of CODAP formula).

It should be stressed again that this study is very preliminary and that more computations will be needed to finalize the design.

4..... CABLE SPECIFICATION

The cable specifications are inspired from those of the LHC quadrupole magnet cable [5]. The cable has 36 strands, a 15.12-mm width, a 1.48-mm mid-thickness, and a 0.9° keystone angle. The transposition pitch length is 100 mm, and the strand diameter is 0.825 mm. As explained above, the critical current is required to be greater than 17,581 A at 10.36 T.

Taking into account a 10% cabling degradation, the virgin strand critical current, I_C^{strand} , must satisfy

$$I_C^{\text{strand}} \geq \frac{17,581}{0.9 \times 36} \approx 543 \text{ A at } 10.36 \text{ T} \quad (7)$$

If we assume further a copper-to-non-copper ratio of 1.4 to 1, the above current intensity specification translates into a critical current density specification in the non-copper, $J_{C,\text{non-Cu}}$, given by

$$J_{C,\text{non-Cu}} \geq 2436 \text{ A/mm}^2 \text{ at } 10.36 \text{ T} \quad (8)$$

Using the usual parametrization of the Nb₃Sn critical surface [9], we derive

$$J_{C,\text{non-Cu}} \geq 1800 \text{ A/mm}^2 \text{ at } 12 \text{ T} \quad (9)$$

Such value is far above the specification for high performance ITER strands (700 A/mm² at 12 T and 4.2 K) [10], but has been achieved recently (and even exceeded) on R&D wires produced by various manufacturers around the world (IGC and Oxford in the USA, SMI in the Netherlands, and possibly MECo in Japan) [11]. Furthermore, DAPNIA/STCM and Alstom/MSA are preparing a 4-year collaboration agreement to develop a high performance Nb₃Sn wire with a goal of 2000 A/mm² at 12 T and 4.2 K. Hence, it seems reasonable to assume that within the time frame of the TESLA project, Nb₃Sn wires meeting the critical current requirement of Eq. (7) will be readily available on the market.

One point of debate is the magnet operating temperature. The promising results on R&D wires mentioned above were obtained at 4.2 K and the Alstom/MSA goal is also at 4.2 K. However, since 1.8-K cryogenics will be available at TESLA, a conservative approach

for the present time is to take advantage of it and to build more margin in the magnet design. Thus, the operating temperature is set to 1.8 K.

5..... CRYOGENICS

5.1 OVERVIEW

The cryogenics of the TESLA quadrupole magnets deals with the cryostat that supports the cold masses of the magnet doublets on each side of the collision point (see Figure 1) and the refrigeration system connected to it.

5.2 CRYOSTAT

A cross sectional view of the cryostat is shown in Figure 12. It is made up of: (1) a stainless steel vacuum vessel with an outer diameter of 355 mm and a overall length of 4200 mm, (2) an aluminum shield cooled with helium gas at 40-50 K, (3) the quadrupole magnet cold masses Q3 and Q4 in their inertia tube with an electrical bus, (4) a set of supporting tie rods and (5) the required tubing for cooling the cold masses. The cold masses and the shields will be super-isolated, respectively, with 10 and 30 layers of double aluminized mylar sheets. Salient dimensions of the various components are summarized in Table 1.

Table 1 Salient dimensions of various items.

Item	Overall length	Outer Diameter
Cryostat	4200	355
Cold mass Q3	1700	250
Cold mass Q4	1000	250

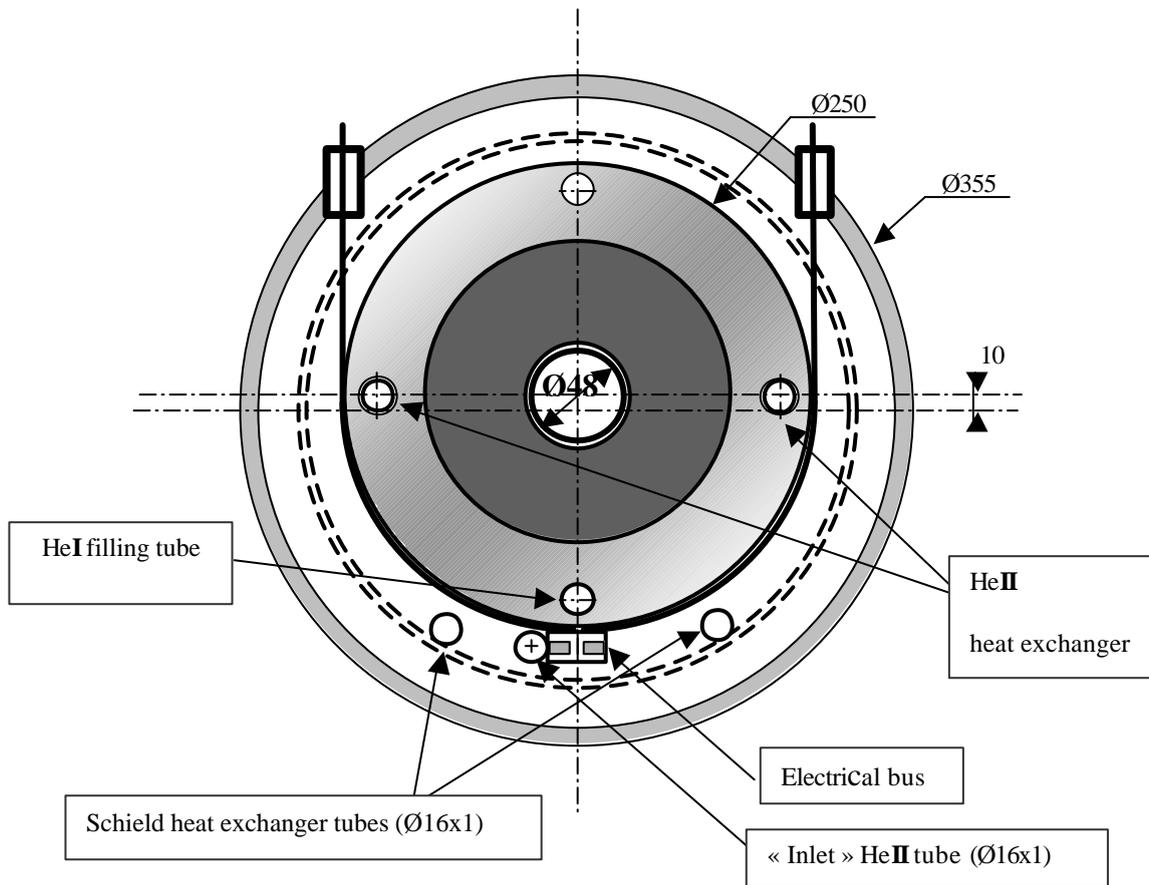


Figure 12 Cross sectional view of quadrupole magnet cryostat.

5.3 REFRIGERATION

The quadrupole magnet coils are in a pressurized bath of helium II at 1.8 K, which is cooled by an internal saturated Helium II loop. The two cold masses are equipped with two copper tubes Ø16x1 connected in parallel (mass flow rate of 0.42 g/s for a heat load of 10 W). The thermal resistance of each tube is roughly 55 W/m, taking into account the Kapitza resistance on tube wall, and thus for a heat load of 3 W/m a $\Delta T < 0.03$ K.

As illustrated in Figure 13, a cryogenic satellite is connected to the cryostat through a cryogenic transfer line with pipes feeding it with fluids: helium gas at 50-70 K, liquid helium I, liquid helium II and a busbar supplying the electrical current.

The main components of the satellite, except its vacuum vessel and super-isolated shield are:

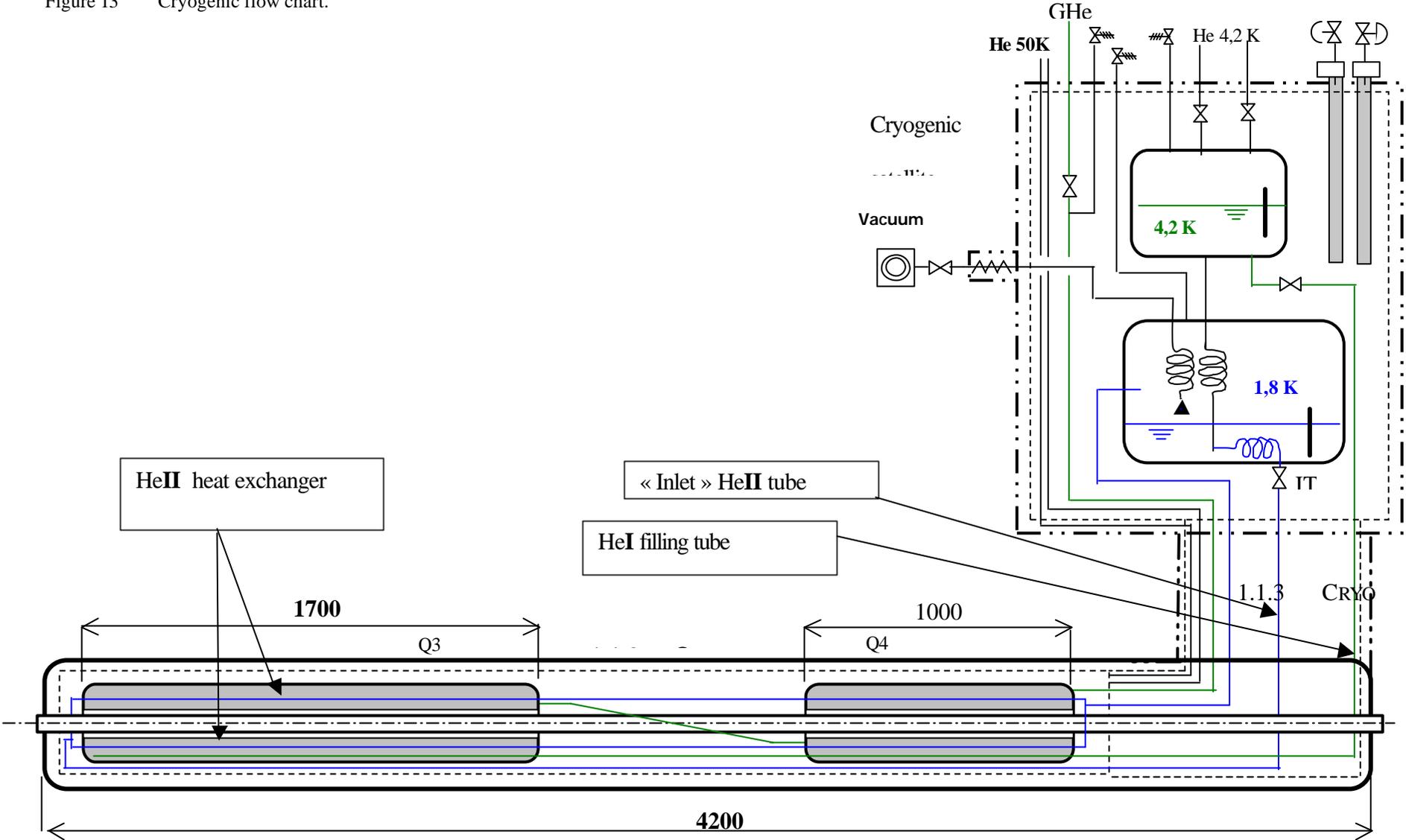
- (1) two 15 kA current leads that have control flow valves,
- (2) a 1.8 K saturated helium II storage vessel connected to an outside pump with an on-line electrical heater (1 kW). A liquid/vapor heat exchanger followed by a liquid/liquid heat exchanger cools the liquid helium I before the Joule-Thomson (JT) valve. The liquid helium II level is controlled by the JT valve and temperature of the saturated helium II bath is controlled by the pumping system ($P_{\text{sat}} = 1640 \text{ Pa}$ for $T_{\text{sat}}=1.8 \text{ K}$). The inlet tube of the saturated helium II loop is cooling also the electrical bus.
- (3) A 4,2 K saturated liquid vessel stores helium I and supplies the internal helium II cooling loop or is used to fill up the cold mass vessels.

5.4 HEAT LOADS (PER CRYOSTAT)

Table 2 Estimated heat loads.

	Cryostat	Transfer line	Satellite
40-50K shield	20 W	5 W	5 W
4.2 K	-		3 g/s
1.8 K	10 W	1 W	4 W

Figure 13 Cryogenic flow chart.



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