Passive sampling techniques for monitoring pollutants in water

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We review the state of the art in using passive sampling technology for environmental monitoring of waterborne organic and inorganic pollutants. We discuss strategies for sampler design, calibration, in situ sampling and quality-control issues, and advantages and challenges associated with passive sampling in aqueous environments. We then review typical applications of passive samplers in assessing the aquatic environment. [©] 2005 Elsevier Ltd. All rights reserved.

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Abbreviations: ASV, Anodic stripping voltammetry; BTEX, Benzene, toluene, ethyl benzene and xylene; DET, Diffusion equilibrium in thin films; DGT, Diffusive gradient in thin films; GC, Gas chromatography; HPLC, High-performance liquid chromatography; LDPE, Low-density polyethylene; MESCO, Membrane-enclosed sorptive coating; nd-SPME; Negligible depletion solid-phase microextraction; NOM, Natural organic matter; OSPAR, The Convention for the Protection of the Marine Environment of the North-East Atlantic; PAH, Polycyclic aromatic hydrocarbon; PCB, Polychlorinated biphenyl; PCDD, Polychlorinated dibenzo[p]dioxin; PCDF, Polychlorinated dibenzo[p]furan; PDB, Polyethylene diffusion bag; PDBS, Passive diffusion bag sampler; PIMS, Passive integrative mercury sampler; PLM, Permeation liquid membrane; POCIS, Polar organic chemical integrative sampler; PRC, Performance reference compound; QA, Quality assurance; QC, Quality control; SBSE, Stir-bar sorptive extraction; SLM, Supported liquid membrane; SLMD, Stabilised liquid-membrane device; SPATT, Solid-phase adsorption toxin tracking; SPMD, Semi-permeable membrane device; SPME, Solid-phase microextraction; SVOC, Semi-volatile organic compound; TLC, Thin-layer chromatography; TRIMPS, Trimethylpentane-containing passive sampler; TWA, Time-weighted average; VOC, Volatile organic compound

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1. Introduction

It is necessary to monitor pollutants in the aquatic environment to satisfy the requirements of legislative frameworks and directives, as many of these compounds can pose a threat to both human health and ecosystems. A number of toxic compounds have been designated priority pollutants [e.g., those on lists of the US Environmental Protection Agency (EPA) and the Water Framework Directive of the European Union (EU)] and their measurement is necessary to ensure that water-quality standards are maintained. Sampling and analysis of such a broad range of organic (e.g., chlorophenols, organo- chlorine pesticides, polyaromatic hydrocarbons, polychlorinated biphenyls) and inorganic (e.g., heavy metals and some of their organo-metallic species) compounds represents an ongoing challenge to the environmental chemist.

Most aquatic monitoring programmes rely on collecting discrete grab, spot or bottle samples of water at a given time. Often, where pollutants are present at only trace levels, large volumes of water need to be collected. The subsequent laboratory analysis of the sample provides only a snapshot of the levels of pollutants at the time of sampling. However, there are drawbacks to this approach in environments where contaminant concentrations vary over time, and episodic pollution events can be missed. One solution to this problem is to increase the frequency of sampling or to install automatic sampling systems that can take numerous water samples over a given time period. This is costly and in many cases impractical, since a secure site and significant pre-treatment of water are required. Such systems are rarely used in widespread monitoring campaigns. Spot sampling yields different apparent concentrations of pollutants depending on the pre-treatment applied (e.g., filtering) and does not provide information on the truly dissolved, bioavailable fraction of the contaminants.

Another approach that yields information on biologically relevant concentrations of pollutants uses biota. A number of test species can be used, depending on the water body being investigated. These organisms can be deployed for extended periods of time, during which they passively bioaccumulate pollutants in the surrounding water. Analysis of the tissues or lipid extracts of the test organism(s) can give an indication of the equilibrium level of waterborne contamination. A number of factors can influence the results – metabolism, depuration rates, excretion, stress, viability and condition of test organism. Furthermore, extraction of analytes from the tissue of animals prior to instrumental analysis is complex.

Estimates of pollutant concentrations in water can also be made by measuring concentrations in benthic sediments and then using equilibrium distribution coefficients to derive levels of dissolved analytes. This approach is limited by the assumption of equilibrium between the sediments and the water column, and the potential effects of organic carbon quality differences among sediments or the formation of non-extractable, sediment-bound residues that are not accounted for in current equilibrium-partition models.

In the last two decades, alternatives have been sought to overcome some of these difficulties. Of these, passive sampling methods have shown much promise as tools for measuring aqueous concentrations of a wide range of priority pollutants. Passive samplers avoid many of the problems outlined above, since they collect the target analyte in situ and without affecting the bulk solution. Depending on sampler design, the mass of pollutant accumulated by a sampler should reflect either the concentration with which the device is at equilibrium or the time-averaged concentration to which the sampler was exposed. Such devices have been available for monitoring air quality since the early 1970s. These diffusion-based dosimeters have been employed extensively by industry to measure toxic chemicals in workplace air.

Later, the principles of passive dosimetry were applied in monitoring in aqueous environments. Milestones in the development of passive sampling devices for monitoring of water pollutants are shown in [Fig. 1](#page-1-0).

This article reviews the state of the art of different passive sampling methods that have been developed to measure both organic and inorganic pollutants in water and highlights their range of applicability. Their potential for use in monitoring programmes is considered alongside other issues, such as quality control and detection limits. We discuss recent developments to extend their use (e.g., extracts from the devices being incorporated into bioassay-based ecotoxicology tests), challenges and limitations of the technology.

2. Principles

Passive sampling can be defined in its broadest sense as any sampling technique based on free flow of analyte molecules from the sampled medium to a receiving phase in a sampling device, as a result of a difference between the chemical potentials of the analyte in the two media. The net flow of analyte molecules from one medium to the other continues until equilibrium is established in the system, or until the sampling period is stopped [\[1\]](#page-20-0). Sampling proceeds without the need for any energy sources other than this chemical potential difference.

Analytes are trapped or retained in a suitable medium within the passive sampler, known as a reference or receiving phase. This can be a solvent, chemical reagent or a porous adsorbent. The receiving phase is exposed to the water phase, but without the aim of quantitatively extracting the dissolved contaminants. Pollutant adsorption or absorption from water into most passive sampling systems generally follows the pattern shown in Fig. 2. The exchange kinetics between a passive sampler and water phase can be described by a first-order, onecompartment mathematical model:

$$
C_{\rm S}(t) = C_{\rm W} \frac{k_1}{k_2} (1 - e^{-k_2 t}), \tag{1}
$$

where $C_S(t)$ is the concentration of the analyte in the sampler at exposure time t, C_W is the analyte concentration in the aqueous environment, and k_1 and k_2 are the uptake and offload rate constants, respectively. Two main accumulation regimes, either kinetic or equilibrium, can be distinguished in the operation of a sampler during field deployment.

2.1. Equilibrium-passive samplers

In equilibrium sampling, the exposure time is sufficiently long to permit the establishment of thermodynamic equilibrium between the water and reference phases. In this situation, equation (1) reduces to:

$$
C_{\rm S} = C_{\rm W} \frac{k_1}{k_2} = C_{\rm W} K. \tag{2}
$$

Knowledge of the phase-water partition coefficient (K) allows estimation of dissolved analyte concentration. An overview of equilibrium-passive sampling devices has been published by Mayer et al. [\[2\].](#page-20-0) The basic requirements of the equilibrium-sampling approach are that stable concentrations are reached after a known response time, the sampler capacity is kept well below that of the sample to avoid depletion during extraction and the device response time needs to be shorter than any fluctuations in the environmental medium. Passive diffusion bag samplers (PDBSs) have been used extensively for monitoring volatile organic compounds (VOCs) in water [\[3,4\]](#page-20-0).

2.2. Kinetic passive samplers

With kinetic sampling, it is assumed that the rate of mass transfer to the reference/receiving phase is linearly

proportional to the difference between the chemical activity of the contaminant in the water phase and that in the reference phase. In the initial phase of sampler exposure, the rate of desorption of analyte from the receiving phase to water is negligible, the sampler works in the linear uptake regime, and equation [\(1\)](#page-2-0) reduces to:

$$
C_{\rm S}(t) = C_{\rm W} k_1 t. \tag{3}
$$

Equation (3) can be rearranged to an equivalent relationship:

$$
M_{\rm S}(t) = C_{\rm W} R_{\rm S} t,\tag{4}
$$

where $M_S(t)$ is the mass of analyte accumulated in the receiving phase after an exposure time (t) and R_S is the proportionality constant (sampling rate), which is the product of the first-order rate constant for uptake of pollutant (k_1) and the volume of water that gives the same chemical activity as the volume of receiving phase. R_S may be interpreted as the volume of water cleared of analyte per unit of exposure time by the device.

When R_S is known, C_W [the time-weighted average (TWA) concentration of a pollutant in the water phase] may be calculated from the sampling rate (R_S) , exposure time (t) and the amount $(M_s(t))$ of the analyte trapped by the receiving phase. For most devices operating in the kinetic mode, R_s does not vary with C_W , but is often affected by water flow or turbulence, temperature and biofouling. The advantages of kinetic or integrative sampling are that they sequester contaminants from episodic events commonly not detected with spot sampling, and can be used where water concentrations are variable. They permit measurement of ultra-trace, yet toxicologically relevant, contaminant concentrations over extended time periods.

2.3. Sampler design

Although many different types of kinetic passive sampler exist, nearly all share common design characteristics, the most important being the presence of a barrier between the sampled medium and the receiving phase. The barrier should determine the rate at which analyte molecules are collected at a given concentration. The barrier may also define the selectivity of the sampler and restrict certain classes of analyte or species sampled. Based on the properties of the barrier, samplers fall into one of the two categories – diffusion-based or permeation-based devices [\[1\]](#page-20-0). The sampling process is similar for both. Once exposed to water, they collect analyte molecules reaching the receiving phase by diffusion through a static layer of water contained in well-defined opening(s) in the sampler (diffusion samplers), or by permeation through a porous or non-porous membrane (permeation samplers).

The uptake rate of analytes depends on the sampler design, physicochemical properties of the analytes and environmental variables (i.e., water turbulence, water temperature and fouling). Passive samplers are designed to maximise the amount of analyte sampled in order to detect the generally low levels of analytes present in water, whilst ensuring a quantitative correlation between the mass of chemical separated and its concentration in the sampled medium.

Diffusional kinetic samplers mostly use a ''tube'' design, where the receiving phase is located inside a long, narrow inert tube or a capillary. The space between the edge of the sampler and the surface of the receiving phase, characterised by a diffusion distance (L), is filled with a stagnant layer of the sampled medium, and this defines the sampling rate. To avoid fluctuations in L, caused by the disturbance of the stagnant diffusion layer by facial water velocity/turbulence, tube-type diffusion samplers are characterised by a relatively low ratio of surface area of the receiving phase A to L. Since the amount of analyte sampled is directly proportional to the surface area of the sampler, tube-type samplers are generally less sensitive than so-called badge-type samplers, characterised by a high A/L ratio. The tube design is usually used in air monitoring. However, sampling kinetics in flat badge-type samplers with a large surface area are more affected by fluctuations in water velocity. To alleviate the impact of these fluctuations, a diffusionlimiting membrane is generally used to separate the receiving phase from the sampled medium and to control the mass transfer of analyte to the receiving phase. In water monitoring, badge-type samplers predominate.

2.4. Calibration of passive samplers

The theoretical background of passive sampling in water has been described previously [\[1,5–7\]](#page-20-0). The substancespecific kinetic constants, k_1 and k_2 , and the distribution coefficient, K, can be determined in two ways. In theory, kinetic parameters characterising the uptake of analytes can be estimated using semi-empirical correlations between mass-transfer coefficients, physicochemical properties (mainly diffusivities in various media) and hydrodynamic parameters [\[8\].](#page-20-0) However, because of the complexity of the water flow around passive sampling devices during exposure (usually non-streamlined objects), it is often difficult to estimate uptake parameters from first principles. For K, which characterises the affinity of a pollutant to the receiving phase relative to water, more substance-specific information is usually available from the literature.

In a practical approach, calibration of passive sampling exchange kinetics is performed in the laboratory at known exposure concentrations [\[9–12\]](#page-20-0). To predict TWA water concentrations of contaminants from levels accumulated in passive samplers, extensive calibration studies are necessary to characterise the uptake of chemicals under various exposure conditions. Uptake kinetics of chemicals depends upon not only the physicochemical properties of the diffusand, but also the sampler design and environmental variables, such as temperature, water turbulence and biofouling of the sampler surface [\[13,14\]](#page-21-0).

2.5. Environmental factors affecting passive sampling It is important to consider the mechanisms of the exchange process between the aqueous phase and the sampler components. The rate-limiting step in the uptake to the receiving phase (in the absence of fouling) may be controlled by diffusion in the diffusion-limiting membrane or across the aqueous diffusive boundary layer at the membrane–water interface [\[15\]](#page-21-0). Water turbulence affects the thickness of the unstirred layer of water that forms part of the diffusion-limiting barrier near the sampler surface, and consequently also affects the mass transfer of the analytes. The rate-limiting step depends on the type and properties of the membrane, the environmental conditions prevailing during sampling and the properties of the compound being sampled.

A number of methods have been developed to compensate for the effect of environmental variables on the sampler performance. Booij et al. [\[16,17\]](#page-21-0) described a method to estimate the uptake kinetics in both laboratory and field situations by spiking devices prior to exposure with a number of performance reference compounds (PRCs) that do not occur in the environment. Where factors influencing uptake kinetics affect the offloading kinetics of PRCs in an identical manner, the release rate of these compounds is a measure of the exchange kinetics between the sampler and water, and can be used in field exposures to compensate for variations in environmental conditions.

2.6. Biofouling

Unprotected surfaces submersed in water eventually become colonised by bacteria and various flora and fauna that may ultimately form a biofilm. The thickness of this biofilm varies from not only exposure to exposure but also spot to spot on the same diffusion-limiting membrane. The composition of biofilms varies significantly depending on the aquatic system. Biofouling can affect the overall resistance to mass transfer by increasing the thickness of the barrier and by blocking any water-filled pores in the diffusion-limiting membranes. Colonising organisms may damage the surface of membranes, if made of a degradable material. Huckins et al. [\[18\]](#page-21-0) reported 20–70% impedance in uptake of polyaromatic hydrocarbons (PAHs) in severe cases, but also showed that, for biofouled semi-permeable membrane devices (SPMDs), PRCs can be applied to correct for biofouling during deployment. Their model describing the mass transfer in a biofilm indicates that, ideally, it behaves like an immobilised water layer, with a resistance independent of the biofilm/water partition coefficient, which would mean a similar mobility of compounds in biofilm, independent of their hydrophobicity [\[18\].](#page-21-0) The problem of sampler fouling may be reduced by selecting suitable construction materials. For example, polyethersulphone used in one design of the Chemcatcher and in the polar organic chemical integrative sampler (POCIS) is less prone to fouling than polyethylene used in SPMDs [\[19\]](#page-21-0). In addition, certain solvent-filled membrane devices are protected from fouling by slow seeping of the foulinginhibiting solvent (e.g., n-hexane) from the sampler during exposure. Protective screens made of copper or bronze mesh have also been shown to inhibit biofouling; however, their use is restricted when monitoring for heavy metals.

3. Passive sampling devices

Passive samplers usually combine sampling, selective analyte isolation, pre-concentration and, in some cases, speciation preservation in one step. They simplify the operations performed at the sampling site. They eliminate the need for an energy/power supply and allow the entire sampling set-up to be simplified and miniaturised. Once the sample is collected, further steps in its processing are usually the same as for other sampling/sample preconcentration methods in analysis. They include extraction/desorption of the analytes, final instrumental analysis and processing the data.

A review of passive samplers used for monitoring pollutants in various media has been published by Namiesnik et al. [\[20\].](#page-21-0) [Tables 1 and 2](#page-5-0) present an overview of devices used to measure organic and inorganic contaminants in water. In the following sub-sections, we present in detail several (but not all) samplers with a potential for use in environmental monitoring programmes to illustrate the manifold applications of this technology.

3.1. Passive samplers for organic pollutants

3.1.1. Semi-permeable membrane devices. SPMDs comprise lay-flat tubing made of low-density polyethylene (LDPE) filled with a high-molecular weight lipid, typically high-purity synthetic triolein. LDPE is a non-porous material with no fixed pores, only transient cavities with a typical size of 1 nm. This solute size limitation excludes large molecules as well as those that are adsorbed on colloids or humic acids. Only truly dissolved and nonionised contaminants diffuse through the LDPE membrane and can be separated by the sampler. Triolein represents a receiving phase with a high capacity for compounds with octanol/water partition coefficients $log K_{OW} > 3$ [\[21\]](#page-21-0). The design of the SPMD was first published in 1990. Since then, nearly 200 studies have been reported, and this is the most mature technique for sampling organic pollutants [\[22\].](#page-21-0) Several reviews and one monograph have been published on this technology [\[18,23–25\].](#page-21-0)

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3.1.2. Polar organic chemical integrative sampler. The POCIS is used to monitor hydrophilic contaminants, such as pesticides, prescription and over-the-counter drugs, steroids, hormones, antibiotics and personal-care products [\[26\]](#page-21-0). Such compounds are entering water and ecosystems on a global scale and some have been linked with chronic toxicities. POCIS samples from the dissolved phase and thereby enables the biologically available fraction to be estimated. This sampler permits determination of TWA concentration in water over extended periods (several weeks).

The POCIS comprises a solid receiving phase material (sorbent) sandwiched between two microporous polyethersulphone diffusion-limiting membranes. The type of sorbent used can be changed to target specifically certain compounds or chemical classes. Two configurations are commonly used:

- a 'generic' configuration contains a mixture of three solid-phase sorbents (Isolute ENV+ polystyrene divinylbenzene and Ambersorb 1500 carbon dispersed on S-X3 Biobeads); it is used to monitor most pesticides, natural and synthetic hormones, many wastewaterrelated chemicals, and other water-soluble organic chemicals and
- the 'pharmaceutical' configuration contains a single (Oasis HLB) solid-phase sorbent and is designed for drug residues [\[26\]](#page-21-0).

3.1.3. Chemcatcher (organic version). This system uses a diffusion-limiting membrane and a bound, solid-phase receiving phase. Accumulation rates and selectivity are regulated by the choice of both the diffusion-limiting membrane and the solid-phase receiving material; both are supported and sealed in place by an inert plastic housing. For a range of priority pollutant classes, a number of designs are available with different combinations of receiving phase and diffusion-limiting membrane [\[27\]](#page-21-0).

One design is used for the sampling of non-polar organic compounds with $\log K_{\rm OW}$ values greater than 4 [\[27\].](#page-21-0) This uses a 47-mm C_{18} Empore disk as receiving phase and an LDPE diffusion-limiting membrane. The C_{18} Empore disk has a high affinity and capacity for nonpolar organic pollutants. Another design used for the sampling more polar organic contaminants combines a 47-mm C_{18} Empore disk as the receiving phase with a polyethersulphone diffusion-limiting membrane [\[27\]](#page-21-0). Other devices are being developed for a range of emerging pollutants, including alkylphenols, antiinflammatory drugs and other pharmaceuticals, polybrominated flame retardants, steroids, sulphonamides and metals (e.g., mercury, tin and their organometallic species) [\[28\].](#page-21-0)

3.1.4. Negligible depletion-solid-phase microextraction. Solid-phase microextraction (SPME) was developed by Pawliszyn et al. [\[29\]](#page-21-0) as a simple extraction method with several advantages over liquid–liquid extraction and solid-phase extraction. The use of organic solvents is diminished and the SPME technique is simple, precise, and it may be automated easily, and the apparatus is inexpensive. The extraction medium is a thin layer of a polymer coating on an optical silica fibre, with a typical volume of 10–150 nL. Extraction equilibrium may generally be reached in 30 min. The mass of analyte on the fibre can be measured by either gas chromatography (GC) or high-performance liquid chromatography (HPLC). While most applications of SPME aim at the highest possible extraction efficiency, negligible depletion SPME (nd-SPME) represents a specific application to measure free concentrations based on negligible analyte extraction from the sampled matrix. In addition to the advantages of SPME, existing equilibria within the sample remain undisturbed during nd-SPME. The disadvantage of nd-SPME is the small amount of analyte that is available for analysis (typically only a few percent of the total amount in the sample), and this may lead to quantification problems. A review of nd-SPME has been published by Heringa and Hermens [\[30\].](#page-21-0)

3.1.5. Membrane-enclosed sorptive coating. This adaptation of the SPME technique to enable integrative passive sampling of hydrophobic organic pollutants has been reported. The device, referred to as the MESCO (membrane-enclosed sorptive coating), comprises a Gerstel Twister stir bar used for stir-bar sorptive extraction (SBSE) or a silicone polymer rod enclosed in a membrane made of regenerated cellulose. The receiving phases may be surrounded by air or water within the bag [\[31\].](#page-21-0) The miniature MESCO sampling system combines sampling with solventless pre-concentration. The sampler enables direct analysis of the accumulated contaminants by thermodesorption coupled on-line to GC, thereby avoiding time-consuming sample preparation and clean-up. Despite the small surface area and volume of the sampler, its sensitivity is comparable with other passive sampling systems, since the entire amount of analyte contained in the receiving phase is introduced into GC and subsequently detected.

3.1.6. Ceramic dosimeter. The ceramic dosimeter [\[32\]](#page-21-0) uses a ceramic tube as the diffusion-limiting barrier to enclose a receiving phase comprising solid sorbent beads. Recently, the utility of the ceramic dosimeter as a robust groundwater-sampling device was demonstrated for benzene, toluene, ethyl benzenes, xylenes (BTEX) and naphthalenes, using Dowex Optipore L-493 as the receiving phase [\[33\]](#page-21-0). In up to 90 days of sampling in a contaminated aquifer, the ceramic dosimeter showed an excellent performance, as judged by comparing TWA contaminant concentrations derived from dosimeters with average aqueous concentrations determined by

frequent conventional spot-sampling methods. Based on the same principle, researchers proposed using Amberlite IRA-743 as a solid receiving phase for the measurement of PAHs [\[32,34\]](#page-21-0).

3.1.7. Polyethylene diffusion bags. There is potential for loss of volatiles during the collection of VOCs from groundwater. Polyethylene diffusion bag (PDB) samplers help to eliminate this problem [\[35,36\].](#page-21-0) The sampler comprises a membrane sealed in the form of a long cylindrical bag, filled with deionised water. The bag is made of LDPE and acts as a semi-permeable membrane allowing the passage of most chlorinated VOCs. VOCs in groundwater diffuse across the membrane into the de-ionised water in the bag until equilibrium is reached. Typically, PDBs take about 2 weeks to equilibrate in an aquifer [\[37\].](#page-21-0) Once this equilibration has occurred, sample recovery takes place.

3.2. Passive samplers for inorganic pollutants

3.2.1. Dialysis in situ. Equilibrium dialysis is a simple, size-based separation method applicable to the study of trace-metal speciation [\[38\].](#page-21-0) Sampling with a dialysis cell is based on a diffusive flux of species able to pass through the cell membrane towards a small volume of water as the acceptor solution, until equilibrium is reached. Metals associated with colloids and humic acid complexes, which are larger than the pores of the membrane, are excluded [\[39\].](#page-21-0)

3.2.2. Dialysis with receiving resins. An alternative configuration to the above is to add a receiving phase (e.g., a chelating resin) with a high affinity for the species being measured in the cell. Under these conditions, the diffusion rate is theoretically directly proportional to the metal concentration in the water being sampled [\[40\].](#page-21-0) If a suitable chelating resin is selected, the bioavailable metal species can be separated. In this case, diffusion across the dialysis membrane may simulate metal-transport processes across biological barriers. The use of the chelating resin, Chelex 100, showed a measurable, reproducible uptake of the soluble fraction of Cd, Pb and Zn at low ambient water concentrations [\[41\]](#page-21-0). Coefficients of variations were lower than for mussels, making this resin a promising acceptor phase for the measurement of dissolved metal species in sea-water. These devices have also been deployed in storm-water run-off and variations in the uptake rates of metals could be correlated to hydrological/hydrochemical parameters, such as rainfall volume and pH [\[42\]](#page-21-0).

3.2.3. Liquid membrane devices. Supported liquid membranes (SLMs) pre-concentrate trace elements from water and have been developed to mimic uptake across biological membranes. This system comprises an organic solvent with a complexing agent that is selective for the target element and is immobilised on a thin macroporous hydrophobic membrane (either as a flat sheet or as a hollow fibre with a small lumen) [\[43,44\].](#page-21-0) One side of the membrane is exposed to the aqueous environment, while the other is in contact with a strip solution containing a complexing agent with a higher affinity towards the metals being separated than the one immobilised in the membrane. A proton, an anion or a metal-ion counter gradient drives the transport across the device. The device can be tailored to separate specific metal species by a careful selection of complexing agents or by altering the lipophilicity of the diffusion membrane [\[45,46\].](#page-21-0) SLM devices have been used to measure Cd, Co, Cu, Ni, Pb and Zn in natural waters. Effects of turbulence, pH and concentration variations on the performance of SLM devices have been reported [\[47\].](#page-21-0)

The permeation liquid membrane (PLM) device is the result of further development of the SLM. This technique is based on carrier-mediated transport of metals across a hydrophobic membrane. The microporous support is impregnated with a hydrophobic organic solvent and placed between the sample and a receiving solution [\[48\]](#page-21-0). The transport of Cu and Pb complexes through a PLM with a neutral macrocyclic carrier has been described [\[49\].](#page-21-0)

3.2.4. Diffusive gradient in thin films. The diffusive gradient in thin-films (DGT) device is a development of a similar sampler – the diffusion equilibrium in thin-films (DET) device – initially suggested by Davison and co-workers in 1991 [\[50\].](#page-21-0) The first reported use of the improved DGT device was in 1994 for measuring Zn in sea-water. The DGT device comprises a gel-layer incorporating a binding agent (which acts as a solute sink) and a hydrated acrylamide diffusion gel separating it from the water column. This creates a diffusion layer of well-defined thickness. The initial design of the DGT utilised an ion-exchange resin as the receiving phase. Later, Zhang and co-workers [\[51\]](#page-21-0) demonstrated the applicability of the technique to determination of trace metals (Cd, Cu, Fe and Mn) in sea-water. With a chelating resin embedded in the gel layer, metals could be quantified as low as 4 pmol/L after deployment for 1 h.

The subsequent refinement of the design and the extended range of inorganic pollutants that may be sampled indicate the versatility and the widespread use of the DGT device. In principle, it is possible to sample any labile species for which a suitable binding agent can be embedded into the receiving phase gel.

3.2.5. Passive integrative mercury sampler. Attempts have been made to use the passive integrative mercury sampler (PIMS), originally designed for air sampling, to sample neutral Hg species in water [\[52\].](#page-21-0) The device comprises lay-flat LDPE tubing containing a reagent mixture of nitric acid and gold stock solution. Experiments were performed in simulated freshwater and sea-water environments. The uptake rates remained linear for 2 weeks and preliminary results indicate that sampling of neutral Hg species from water is feasible. Sampling in freshwater was more effective than in seawater, likely to be because a larger fraction of the total Hg in sea-water was present as charged chloro-anion complexes that could not readily permeate through the membrane.

3.2.6. Chemcatcher (inorganic version). An alternative configuration of the Chemcatcher (see Section 3.1.3) has been developed for the separation of metals. The device comprises a commercially available 47 mm diameter chelating extraction disk as receiving phase and a cellulose acetate diffusion-limiting membrane [\[53\]](#page-21-0). The sampler has been used to monitor Cd, Cu, Ni, Pb and Zn, in various aquatic environments, such as a storm-water pond, where the uptake of metals was compared with flow-weighted bottle samples. Results indicated a good correlation with the electro-available Cu fraction but were somewhat less clear for Zn [\[53\]](#page-21-0).

The diffusion-limiting membrane can be treated with a low surface-energy coating (e.g., polyfluorinated sulphonic acid polymer (Nafion)) to reduce biofouling on the surface of the membrane. The diffusion characteristics of the membrane, the influences of water turbulence and the radius of metal ions monitored have been investigated [\[54\].](#page-21-0)

4. Applications of samplers

The first publications on the use of passive samplers to monitor aquatic contaminants were in 1980s ([Fig. 1](#page-1-0)) and these devices have since received widespread recognition as effective tools in environmental research. Passive sampling technology is widely applicable in monitoring studies and the results obtained can be interpreted at different levels of complexity. Passive samplers have been employed in field studies aimed at:

- (a) screening for the presence and absence of pollutants;
- (b) investigating temporal trends in levels of waterborne contaminants;
- (c) monitoring spatial contaminant distribution and tracing point and diffusive pollution sources;
- (d) speciation of contaminants;
- (e) assessing pollutant fate and distribution between environmental compartments;
- (f) measuring TWA concentrations of waterborne pollutants;
- (g) comparing contaminant patterns in biota and passive samplers – biomimetic sampling to estimate organism exposure; and,

(h) assessing toxicity of bioavailable pollutants in extracts from the receiving phase of passive samplers.

[Tables 3 and 4](#page-13-0) illustrate the different field applications. These tables are not intended to be comprehensive, but rather to give the reader an overview of the variety of applications. A detailed review of the organic contaminant classes and aqueous matrices that can be sampled by passive samplers was recently published by Stuer-Lauridsen [\[55\].](#page-21-0)

4.1. Use in chemical monitoring

There are several advantages in using passive samplers for monitoring pollutants in water including:

- (a) non-mechanical or passive operation;
- (b) ability to sample large volumes of water and
- (c) reduced effort required for deployment and sample processing compared to other commonly used methods.

Currently available passive sampling devices are applicable to monitoring chemicals with a broad range of physicochemical properties ([Fig. 3](#page-18-0)) and the detection limits obtained or the lowest measured concentrations ([Fig. 4](#page-18-0)) suggest that passive samplers may find application in monitoring programmes.

Stuer-Lauridsen [\[55\]](#page-21-0) indicated that passive sampling devices can be used to monitor more than 75% of the organic micropollutants listed in water-quality criteria of the EU and US, the EU Water Framework Directive and the recommendations of The Convention for the Protection of the Marine Environment of the North-East Atlantic (OSPAR).

4.2. Contaminant speciation

Speciation of environmental contaminants includes not only physicochemical speciation of the forms in which analytes are present in the sampled matrix (e.g., freely dissolved, colloidal and particle-bound forms), but also chemical speciation (e.g., the valency state of metals in the sampled water). Trace metals are present in water in various forms (hydrated ions, and inorganic and organic complexes) together with species associated with heterogeneous colloidal dispersions. The particulate phase also contains elements in a range of chemical associations, from weak adsorption to binding in the mineral matrix. These species coexist, although they may not necessarily be in thermodynamic equilibrium.

The difficulty in differentiating the various forms arises from the low levels present in natural waters. The fractionation of species is recognised as an essential step in assessing bioavailability and toxicity in water. A problem is that solution equilibria may change after sample collection through adsorption or desorption of analytes to particulate and colloidal surfaces. A representative

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value is particularly difficult to identify through conventional sampling procedures in environments where concentrations fluctuate [\[56\]](#page-21-0).

4.2.1. Organic contaminants. Passive samplers can be applied to characterise the distribution of organic contaminants between particulate, dissolved and colloidal phases in the water column [\[57–59\]](#page-21-0). The selectivity of devices may be adjusted to sample a desired fraction of an analyte present by choosing membrane materials with desired properties (e.g., pore size and charge on the surface).

Most passive samplers collect only the truly dissolved fraction of chemicals, since: (a) the truly dissolved molecules become separated from colloids and particles during their diffusion across the membrane that separates water from the receiving phase [\[21\];](#page-21-0) and, (b) only

dissolved molecules are sorbed by the receiving phase [\[30\].](#page-21-0)

4.2.2. Inorganic contaminants. Passive samplers have been used to gain understanding of the species of metals in the aquatic environment. Speciation of metals with the DGT device relies on two effects: the relative difference in diffusion coefficients; and, the relative difference in affinity to the binding agent between the species to be characterized. It is possible to differentiate between inorganic labile species and organic labile species by employing a systematic variation of diffusion gel pore sizes, resulting in a size-discriminating uptake in a similar fashion to voltammetry. However, diffusion coefficients of the model species have to be determined individually to make accurate measurements of the concentration of the labile species [\[60\].](#page-21-0)

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4.3. Quantification of concentrations in water

Passive sampling methods can be used to calculate the concentrations of compounds in the aqueous phase, using the principles described in Section 2. [Fig. 5](#page-19-0) illustrates the way in which integrative passive samplers can provide representative information on TWA contaminant concentrations over a long period of time with a sampling frequency lower than in spot sampling. However, it is important to recognise that, in most cases, the aqueous concentration estimated using passive samplers reflects only the truly dissolved contaminant fraction and is not necessarily equal to the concentration measured in spot samples, particularly in very hydrophobic compounds in the presence of elevated levels of dissolved organic matter. Nevertheless, the comparison is possible, if all species and fractions of contaminants present in the sampled matrix are characterised (see Section 1).

In many aquatic systems, contaminant concentrations are not constant, but fluctuate or occur in the form of unpredictable pulses. Concentrations reflected by integrative passive samplers are TWAs over the exposure period, but more research is needed to quantitate the uptake in passive samplers in scenarios involving pulsed and discontinuous exposure. Such research will provide sufficient evidence of realistic concentration estimates using passive samplers and convince the regulators of the application of passive samplers in monitoring programmes.

4.4. Estimate of organism exposure

Sijm et al. [\[61\]](#page-21-0) reviewed biomimetic passive sampling methods to study the bioavailability of chemicals in soil or sediment. Biomimetic equilibrium sampling approaches using SPME [\[29\]](#page-21-0) and Empore disks can mimic partitioning of contaminants between the pore water and the organism. Both approaches assume that the freely dissolved contaminant concentrations will represent bioavailability. However, for substances that may be biotransformed in the organism, the methods will overestimate the concentration in the organism. For organisms that have several routes of uptake (in addition to via the water phase), the biomimetic method will underestimate the concentration in the organisms.

Biomimetic sampling devices have been applied to sense dissolved sediment pore-water concentrations

Figure 3. Typical hydrophobicity range of organic compounds sampled by selected passive sampling devices (characterised by the value of octanol/water partition coefficient, $log K_{OW}$).

of contaminants [\[62,63\]](#page-21-0) and to estimate the bioaccumulation potential in effluents and surface waters [\[64,65\].](#page-21-0)

4.5. Bioassays

The pre-concentrated extracts obtained from the elution of receiving phases of passive samplers (particularly those used to measure organic pollutants) can subsequently be combined with a variety of bioassay procedures to assess both the level and the biological effects of water contaminants [\[66\].](#page-21-0) In some in vitro bioassays used to assess the health of an ecosystem, problems can occur due to the difficulty of obtaining suitable water samples for testing. For example, most hydrophobic organic contaminants are present in aquatic environment only at trace levels (i.e., $\leq 1 \mu g/L$). The extraction of several litres of water would be required to yield sufficient amounts of analyte for subsequent bioassay.

The use of ''bio-mimetically'' separated extracts from passive samplers can overcome this problem [\[67\].](#page-21-0)

It has been shown that the baseline toxicity of chemicals can be predicted (based on total body residue estimates) from the concentration of contaminants separated by passive samplers [\[68\].](#page-21-0)

5. Quality control

The level of quality control (QC) applied to passive sampling varies with project goals and analytical procedures

Netherlands, in Spring 2004 [\[144\].](#page-22-0)

involved. The application of appropriate QC procedures and parameters is a mandatory consideration in both sampler deployment and subsequent analysis. QC samples should address issues of purity of materials used to construct a device, and potential contamination during transport, deployment, retrieval and subsequent storage. QC protocols are also required for analyte recovery and further processing (enrichment and fractionation operations). Control charts are recommended for monitoring analyte recoveries throughout a project. The QC samples relevant to passive sampler studies include fabrication blanks, process blanks, reagent blanks, field blanks and sampler spikes.

DeVita and Crunkilton [\[69\]](#page-21-0) examined the QC issues associated with using SPMDs for monitoring PAHs in water. Their results showed that QC measures applied to SPMDs met or surpassed conventional guidelines (EPA method 610 for PAHs in water) for precision and accuracy.

However, assessing the accuracy and the trueness of determinations made by passive samplers may prove difficult, as the results may not be directly comparable with total concentrations found in spot samples or by other sampling techniques. This is because only very few methods, other than passive samplers, can truly measure dissolved contaminant fractions.

When environmental conditions at an exposure site differ from laboratory calibration conditions or calibration data are not available, samplers spiked with PRCs serve as a special type of QC sample. These provide information about in situ uptake kinetics [\[16,17\].](#page-21-0)

QC samples involved in using passive sampling devices are shown in [Fig. 6](#page-20-0).

Stuer-Lauridsen [\[55\]](#page-21-0) discussed the quality assurance (QA) that would be required for passive samplers to be accepted in water-quality-monitoring programmes.

6. Future trends

There are several major trends in the future development of passive sampling technology.

The first is towards miniaturisation of devices. Small devices offer the advantages of inexpensive transportation to and from the sampling site, the requirement for small deployment devices and a low consumption of solvents and reagents during their subsequent processing. Moreover, miniaturised devices allow application in situations with limited space and volume of water (e.g., in groundwater boreholes [\[70\]](#page-21-0)). Miniaturisation goes hand in hand with the trend to develop solventless sample-preparation techniques. Passive samplers based on *in situ* analyte preconcentration using SPME or similar techniques allow sample processing (following exposure) using thermal desorption GC [\[31\]](#page-21-0) or solvent microextraction followed by HPLC [\[71\].](#page-21-0) However, the practical application of SPMEbased techniques in in situ passive sampling of aqueous trace contaminants will require their robustness and sensitivity to be further enhanced.

The second trend is the development of passive sampling technology to monitor a wider range of chemicals. Recently, attention has been focused on compounds with medium-to-high polarity (e.g., polar pesticides and drugs [\[26\]\)](#page-21-0).

Precise calibration of passive sampling devices for monitoring trace metals is essential for quantifying the various metal species and complexes found in water.

This requires knowledge of the uptake kinetics of different metal moieties. Configuration of specific devices for monitoring well-defined fractions of metals will increase their potential as regulatory tools.

A further challenge is to improve robustness by reducing or controlling the impacts of environmental conditions and biofouling on the sampler performance. Internal and external PRCs are being tested for improving the accuracy of TWA concentrations of contaminants.

Another trend is the coupling of chemical and biological analysis of samples collected using passive samplers, with detection and identification of toxicologically relevant compounds. The marriage of passive samplers and bio-marker and bio-indicator tests offers many avenues of investigation to provide information concerning the relative toxicological significance of waterborne contaminants.

Finally, the development of efficient QA, QC and method-validation schemes for passive sampling techniques is essential to gain broader acceptance for the technology in regulatory programmes.

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