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NRCC-44680

A version of this paper is published in / Une version de ce document se trouve dans :
Proceedings of the International Conference on Underground Infrastructure Research,
Kitchener, Ontario, June 11-13, 2001, pp. 1-6

www.nrc.ca/irc/ircpubs



WARP — Water Mains Renewal Planner

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1 INTRODUCTION

The effective planning of water distribution system renewal requires accurate quantification of the structural deterioration of water mains. As water distribution systems comprise hundreds and even thousands of buried pipes, direct inspection of all of them is often prohibitively expensive. Identifying water main breakage patterns over time is an effective and inexpensive alternative to measuring the structural deterioration of a water distribution system.

WARP is a prototype application under development at the National Research Council of Canada. In its current form as a prototype it is being developed as a MS-Excel application (later to be converted to a dedicated program). It is intended to demonstrate how the most promising breakage analysis models can be brought together to form a decision support tool. Currently, WARP consists of three modules:

(a) analysis of water main breakage patterns, (b) short-term operational forecasting and (c) long-term renewal planning. A fourth module will be added to facilitate prioritisation of individual water mains for renewal.

WARP observes three types of factors affecting water main breakage rates. The first type is termed background ageing, which is a result of corrosion and other steady, continuous deterioration processes. The second type consists of cyclical environmental effects such as temperature and soil moisture. The third type comprises operational factors such as water main replacement rates and the rate of cathodic protection retrofit.

In the first module WARP uses an approach proposed by Kleiner and Rajani (2000a) to distinguish the effects of these three types of factors. In the second module WARP uses Fourier analysis to model and forecast the cyclical environmental (second type) factors affecting pipe breaks. This forecast is

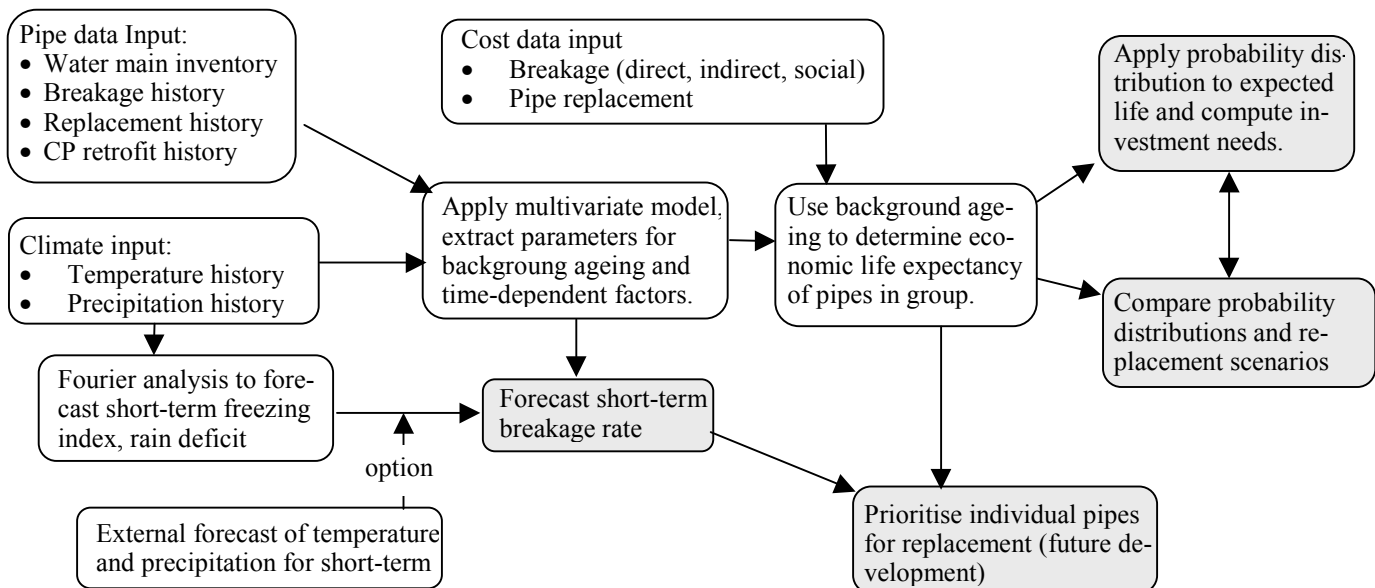


Figure 1. Schematic description of WARP

subsequently used to forecast water main breaks in the short-term (3 to 4 years) (Kleiner and Rajani 2000b). In the third module WARP uses the background ageing rates identified in the first module, to project long-term budgetary needs for water main renewal. The user can select various probability distributions for water main replacement rates, examine various assumptions and strategies and compare their impact on the long-term capital investment needs. A schematic description of WARP is presented in Figure 1.

The rest of this paper is organised as follows. Section 2 discusses briefly the nature of time-dependent factors affecting pipe breaks and their representation in the model. Section 3 describes how climate forecasts are made by WARP. Section 4 describes briefly how WARP uses the model and climate forecast to make short-term pipe break forecast. Section 5 discusses aspects of long-term planning of water main renewal. Section 6 describes WARP's data requirements.

2 TIME-DEPENDENT FACTORS AFFECTING WATER MAIN BREAKS

Kleiner and Rajani (2000a & 2000b) have proposed a multi-variate exponential (or an alternative power model) to consider time-dependent cyclical and operational factors in predicting water main breaks.

$$N(\underline{x}_t) = N(\underline{\bar{x}}_{t_0})e^{\underline{a} \cdot \underline{x}_t^T} \quad (1)$$

where \underline{x}_t = vector of time-dependent covariates prevailing at time t , $N(\underline{x}_t)$ = number of breaks resulting from \underline{x}_t , \underline{a} = vector of parameters corresponding to the covariates \underline{x} ; $\underline{\bar{x}}_{t_0}$ = vector of baseline \underline{x} values at year of reference t_0 . Time-dependent covariates (or “explanatory variables”) could be pipe age, temperature, soil moisture, etc. Parameters $N(\underline{\bar{x}}_{t_0})$ and \underline{a} can be found by regression.

Conceptually, pipe breakage rate can be viewed as a non-decreasing function of time (background ageing), with “noise” that is superimposed upon it by time-dependent effects (Fig. 2). Some of these time-dependent factors are steady while others are transient or cyclical in nature. Natural cyclical effects tend to average out in the long run, however,

when dealing with short data sets, failure to consider their impact can introduce significant bias into results. As well, any short-term (2 to 4 years) forecast of water main breaks, must consider these time-dependent effects.

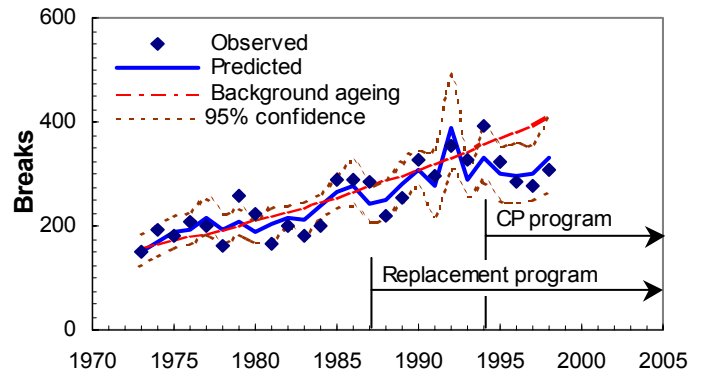


Figure 2. Background ageing and year-to-year variations in water main breaks

Kleiner and Rajani (2000b) provided many references to reported observations concerning the influence of temperature and soil moisture on the frequency of water main breaks. Rajani et al. (1996) developed a pipe-soil interaction model, which explained that buried mains are restrained from movement by the frictional resistance between pipe and soil. Differential temperature change between pipe and soil, and also soil shrinkage due to dryness result in the development of stresses in the pipe. Rajani and Zhan (1996) described the mechanics and circumstances leading to generation of frost loads. They showed that dry soil (expected after an extreme dry season) has low latent heat capacity and will therefore lead to deeper frost penetration.

WARP in its current form is geared more towards cold climates and accounts for the factors age, freezing index (FI), rain deficit (RD) cumulative length of replaced water mains (CLR) and cumulative length of cathodic protection retrofit ($CLCP$). FI is a surrogate measure for the severity of winter and RD is a surrogate measure for soil moisture. RD is considered in two separate forms. Cumulative RD , which is a measure of the average soil moisture over a time period, corresponds to the effects described by Rajani et al. (1996). Snapshot RD , which is a measure of the soil moisture during winter, when the soil is mostly frozen, corresponds to the effects described by Rajani and Zhan (1996).

NRC - CNRC		BREAK HISTORY ANALYSIS		WARP™	
BASIC INPUT					
Water main break analysis		City:	Ottawa	Explanatory variables	
Pipe group:	Cast iron mains	Reference date:	1956	No_breaks	0.04
Specify data availability		From year:	1973	ageing rate for old pipe	3.89%
Water mains breaks	Monthly	To year:	2000	Freezing index (FI)	0.0473
Period for available data (breaks & climate)	Annual	Start year:	1973	Rainfall deficit (RD) - cumulative	0.0206
Water mains break and climate data time frame analysis		End year:	1998	Rainfall deficit (RD) - snapshot	0.0846
Temperature threshold for Freezing Index (FI)	0.0	Coeff. of determination	0.8003	Pipe replacement (CLR)	-6.2812
Time dependent factors		Residual - sum of squares	0.0056	Cathodic Protection (CP)	N/A
Temperature (FI)	<input checked="" type="checkbox"/> Freezing index	Confidence level	95.00%		
Rainfall deficit (RD)	<input checked="" type="checkbox"/> RD - cumulative <input checked="" type="checkbox"/> RD - snapshot				
Pipe replacement program	<input checked="" type="checkbox"/> Pipe replacement	Precipitation data available			
Cathodic protection program	<input type="checkbox"/> Cathodic protection	Replacement data available			
		CP data available			

Figure 3. Basic input screen

In equation (1) FI and RD are expressed as Z-scores, which are the normalised forms of these variables. CLR and $CLCP$ are expressed as a percentage of the population of water mains. Kleiner and Rajani (2000b) provide a detailed description of how all these variables are measured and calculated. In different climates FI may not be relevant but other factors may become important and should be considered.

Equation (1) should be applied to groups of pipes that are relatively homogeneous with respect to their response to the selected set of time-dependent factors. The criteria of grouping the pipes into homogeneous groups can be unique to a distribution system and is often not known a priori. Kleiner and Rajani (1999) described a method to partition water mains into homogeneous groups.

3 SHORT-TERM FORECAST OF CLIMATIC FACTORS

The variables FI and RD have to be forecast as well in order to forecast water main breaks in the short term. FI is calculated from daily temperatures and RD from monthly temperature and precipitation data (Kleiner & Rajani 2000b). Therefore, temperature and precipitation have to be forecast in order to calculate the anticipated breakage rate. These fore-

casts can sometimes be obtained from local climate prediction services. If unavailable, WARP provides a “do it yourself” tool that uses Fourier analysis to forecast temperature and precipitation based on their history. This form of analysis breaks up the historical data into separate harmonic components under the assumption that climate events are harmonic.

The historical variations of the data are transformed to the frequency domain, where one can

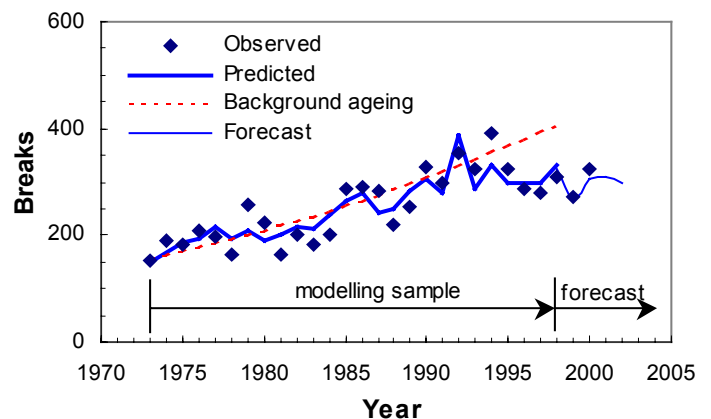


Figure 4. Short-term forecasting of pipe breaks

identify dominant underlying response-frequencies, and subsequently filter out spurious ones. Subsequently, an inverse FFT can be applied to convert

LONG-TERM PLANNING ANALYSIS

WARP™

City: **Ottawa**

Pipe group: **Cast iron mains**

BASIC INPUT
Help

Cost of each break / repair	\$ 6,000	Vintage year	1940
Cost of water loss for each break / event	\$ 500	Reference year	2000
Damage repair costs for other property / event	\$ 200	Remaining pipe length to replace	1898 km
Social cost of each break / event	\$ 200	Maximum replacement period	20 years
Cost of construction per m	\$540 / m	Required investment needs every	5 years
discount rate	3.00%	Estimated ageing rate for new pipe	2.0%

User specified scenario: Linear replacement rate
 starting at increase annually by

User specified scenario: Arbitrary replacement rates

2001	<input style="width: 50px;" type="text" value="10.0 km"/>	2006	<input style="width: 50px;" type="text" value="7.0 km"/>	2011	<input style="width: 50px;" type="text" value="5.0 km"/>	2016	<input style="width: 50px;" type="text" value="4.0 km"/>
2002	<input style="width: 50px;" type="text" value="10.0 km"/>	2007	<input style="width: 50px;" type="text" value="6.0 km"/>	2012	<input style="width: 50px;" type="text" value="5.0 km"/>	2017	<input style="width: 50px;" type="text" value="4.0 km"/>
2003	<input style="width: 50px;" type="text" value="10.0 km"/>	2008	<input style="width: 50px;" type="text" value="5.0 km"/>	2013	<input style="width: 50px;" type="text" value="5.0 km"/>	2018	<input style="width: 50px;" type="text" value="4.0 km"/>
2004	<input style="width: 50px;" type="text" value="9.0 km"/>	2009	<input style="width: 50px;" type="text" value="5.0 km"/>	2014	<input style="width: 50px;" type="text" value="5.0 km"/>	2019	<input style="width: 50px;" type="text" value="4.0 km"/>
2005	<input style="width: 50px;" type="text" value="8.0 km"/>	2010	<input style="width: 50px;" type="text" value="5.0 km"/>	2015	<input style="width: 50px;" type="text" value="5.0 km"/>	2020	<input style="width: 50px;" type="text" value="4.0 km"/>

Figure 5. Data input - costs and user-defined replacement

the filtered data back into the time domain to forecast climate for the desired time period.

4 SHORT-TERM FORECAST OF WATER MAIN BREAKS

Once the parameters of equation (1) are established by regression, and the climate is forecast using Fourier analysis, water main breaks can be forecast for the short term (2 to 4 years). WARP allows the user to toggle variable on and off so that the modelling and the forecasts may be performed with the full set of variables or with a partial set. This feature makes the tool more flexible and adaptable to various conditions (Figs. 3 & 4).

WARP allows also the performance of regression on a sub-set of the observed data and the forecast of breaks that can subsequently be compared to the data that were not used (holdout sample) for regression. In this way the user can see how well the model actually forecasts water main breaks.

WARP allows user flexibility in defining the beginning and the end of the base timestep of 12

months. It often useful to perform the analysis using a timestep period that is based on seasons rather than on the calendar. For example, in Ottawa the timestep that gave the best results was the May-to-April 12 month period, corresponding to the beginning of spring to end of winter period.

5 PIPE AGEING AND LONG-TERM RENEWAL PLANNING

Long-term planning of water main renewal requires accurate estimation of the underlying water main ageing rates in order to identify the time at which it is more economical to replace rather than to continue repairing the pipe. The “true” underlying ageing rate can often be masked by time-dependent factors. By distinguishing between the various factors impacting breakage frequency, WARP can un-masks these true underlying ageing rates. Kleiner & Rajani (2000a) demonstrated how this “un-masking” of the underlying ageing trend is especially important in relatively short data sets, where cyclical envi-

ronmental effects can significantly bias the ageing trend.

Once the ageing rate is determined, WARP uses a method proposed by Kleiner & Rajani (1999) to determine median and variance of the life expectancy of the (presumably homogeneous) population of the pipes being analysed. The user can then assume various probability distributions (Weibull, Gumbel, Herz) of this life expectancy and view the investment needs resulting from these assumptions (Figs. 5, 6)

In addition, the user can apply the KANEW model (Deb 1998), and compare the investment needs resulting from this model to those resulting from the Kleiner & Rajani (1999) approach.

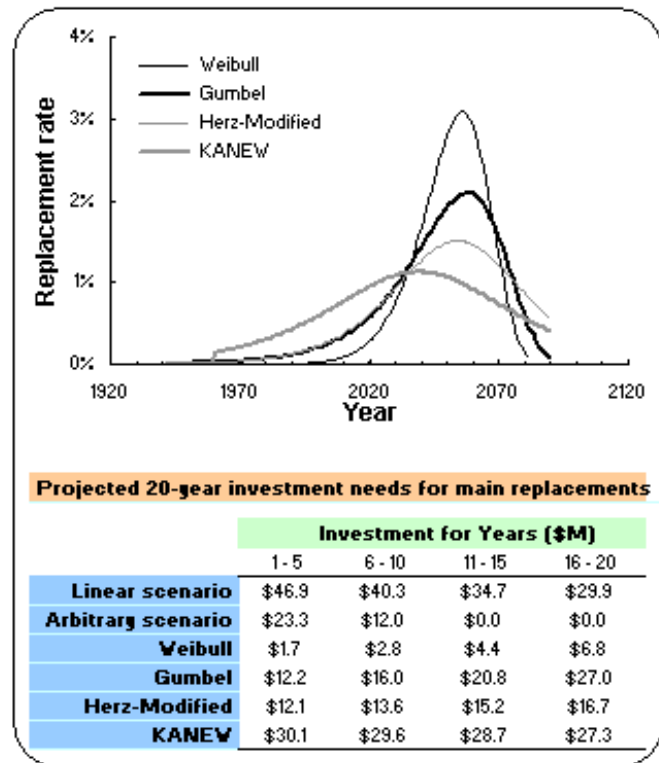


Figure 6. Long-term planning results

The user can also enter arbitrary investment schedules in water main renewal and view how various scenarios are likely to impact total future expenditures (renewal investment plus breakage repair).

6 DATA REQUIREMENTS

WARP requires the following data for each group of pipes to be analysed as a homogeneous population:

- ◆ Historical number of pipe breaks by month (Fig. 7).
- ◆ Average (preferred daily, but monthly will do) temperatures for the period corresponding to the available main breakage data (Fig. 7).
- ◆ Average monthly precipitation for the same period (Fig. 7).
- ◆ Total length of water mains in the group for each year in this period.
- ◆ Total length of water mains replaced in the group, preferably by month, but annual figures will suffice.
- ◆ Total length of water mains in the group retrofitted with cathodic protection, preferably by month, but annual figures will suffice.
- ◆ Geographical latitude of the location of the pipe network (accuracy of one degree is sufficient) to adjust for rain deficit calculations.
- ◆ Cost and economic data including pipe replacement, breakage repair, water loss, social cost of failure and discount rate (Fig. 4).
- ◆ Planning parameters including planning horizon, planning timestep, estimated ageing rate for new pipe, etc. (Fig. 4).
- ◆ For the KANEW model option, point estimates of the survival time of the water main group (three points are required).

7 SUMMARY

The computer application prototype WARP is a decision support tool that currently comprises three modules:

- Analysis of water main breakage patterns that considers time-dependent factors. The influence of each of these factors is quantified to identify deterioration rates of buried water mains as a result of normal (background) ageing.
- Short-term operational forecasting conducted in two steps. The first step is to obtain monthly forecasts for temperature and rainfall from an analysis of historical data (alternatively, forecasts can be obtained from climate centres that study weather dy-

namics). The second step involves forecasting the breakage pattern of mains for the next few years using the failure patterns identified in the first module in conjunction with the climate information derived from step one of this (second) module.

- Long-term renewal planning uses the ageing rate identified in the first module to determine the replacement rate of water mains in the system. The user can compare various patterns of ageing and select the most appropriate one on which to base a long-term replacement strategy.

A fourth module, which allows users to set priorities for the renewal/replacement of individual water mains, will be added in the near future.

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Year	Month	breaks	Temp	Total Precip
1972	1	20	-8.8	96.6
1972	2	18	-11.6	97.1
1972	3	16	-5.8	45.4
1972	4	14	2.1	52.7
1972	5	11	14.2	133.2
1972	6	4	16.8	186.5
1972	7	7	20.5	144.4
1972	8	2	18.5	72.2
1972	9	9	15.3	86.6
1972	10	9	6.1	75.4
1972	11	24	0.2	126.0
1972	12	22	-8.1	55.5
1973	1	16	-7.4	46.3
...
...
1998	5	9	17.5	119.0
1998	6	13	19.2	85.1
1998	7	13	20.8	50.4
1998	8	12	20.5	71.6
1998	9	12	15.7	71.4
1998	10	17	9.3	46.3
1998	11	29	2.9	65.0
1998	12	55	-2.9	5.2

Figure 7. Input of breakage, temperature and precipitation data